September 17, 2014

BOARD OF COUNTY COMMISSIONERS ORANGE COUNTY, FLORIDA ADDENDUM NO. 4 / IFB Y14-7035-PH

ALLISON OAKS 3893A, GREENVIEW PINES 3887, BRADFORD COVE 3290, ROUSE AND UNIVERSITY 3365 AND LENA STREET 3309 PUMP STATIONS IMPROVEMENTS BID OPENING DATE: September 25, 2014

This Addendum is hereby incorporated into the bid documents of the project referenced above. The following items are clarifications, corrections, additions, deletions and/or revisions to and shall take precedence over the original documents. Additions are indicated by <u>underlining</u>, deletions are indicated by <u>strikethrough</u>.

The bid opening remains September 25, 2014 at 2:00 P.M.

A. CLARIFICATIONS

- 1. Q: Appendix A of the Specifications contains a geotechnical report for Rouse and University PS 3365, and Lena Street PS 3309. Are there any geotechnical reports available for the other pump stations?
 - A: There is additional information available for only Allison Oaks PS 3893A and Greenview Pines PS 3887. These documents, which are attached and dated this addendum are named as follows:
 - Geotechnical Engineering Report for Allison Oaks Pump Station, prepared by Nodarse and Associates, Inc.
 - NPDES Groundwater Testing and Database Search for Allison Oaks Pump Station, prepared by Nodarse and Associates, Inc.,
 - Geotechnical Engineering Report for Greenview Pines Pump Station, prepared by Nodarse and Associates, Inc.
 - NPDES Groundwater Testing and Database Search for Greenview Pines Pump Station, prepared by Nodarse and Associates, Inc.

2. Q: Plan Sheet C-101 shows we are to install 6" x 8" curbing with a 4" reveal, should that be 6" x 18"?

A: Yes, the call out on Sheet C-101 should read 6" x 18", not 6" x 8". This Plan Sheet has been corrected in this Addendum

- 3. Q: What type of wet well liner is existing in the Rouse and University PS 3365?
 - A: The existing wet well liner is HDPE. This liner is damaged and is scheduled to be removed in this project.
- 4. Q: It appears that the Rouse and University PS 3365 is the only pump station that has an existing wet well liner, is this correct?
 - A: Yes, the Rouse and University PS 3365 is the only wet well that has an existing wet well liner.

B. PROJECT MANUAL

TABLE OF CONTENTS

Page iv, APPENDICES

Add: Under the heading "APPENDIX A - GEOTECHNICAL REPORT", add the following text:

<u>Geotechnical Engineering Report for Allison Oaks Pump Station, prepared</u> by Nodarse and Associates, Inc.

NPDES Groundwater Testing and Database Search for Allison Oaks Pump Station, prepared by Nodarse and Associates, Inc.,

<u>Geotechnical Engineering Report for Greenview Pines Pump Station,</u> prepared by Nodarse and Associates, Inc.

NPDES Groundwater Testing and Database Search for Greenview Pines Pump Station, prepared by Nodarse and Associates, Inc.

APPENDIX A

Add: Add the above referenced documents to Appendix A of the Specifications, which are attached and dated this Addendum.

C. PROJECT DRAWINGS

SHEET C-101

- Delete: Delete the text that points to the concrete curb that reads "CONST 6" X 8" CONC CURB W/ 4" REVEAL AND WEEP HOLES WHERE APPLICABLE"
- Add: Add in its place the following note: "<u>CONST 6" X 18" CONC CURB W/ 4"</u> <u>REVEAL AND WEEP HOLES WHERE APPLICABLE</u>"

D. ACKNOWLEDGEMENT OF ADDENDA

- a. The Proposer shall acknowledge receipt of this addendum by completing the applicable section in the solicitation or by completion of the acknowledgement information on the addendum. Either form of acknowledgement must be completed and returned not later than the date and time for receipt of proposal.
- b. All other terms, conditions and specifications remain the same.
- c. Receipt acknowledged by:

Authorized Signature

Date Signed

Title

Name of Firm

Geotechnical Engineering Report

Allison Oaks Pump Station No. F3215

Winter Park, Florida

September 21, 2012 Terracon Project No. AK127001

Prepared for:

Orange County Public Utilities-Engineering Division Orlando, Florida

Prepared by:

Nodarse & Associates A Terracon Company Winter Park, Florida

Offices Nationwide Employee-Owned nodarse.com terracon.com



September 21, 2012

Orange County Public Utilities – Engineering Division 9150 Curry Ford Road Orlando, Florida 32815



Attn: Mr. Jeff Nazario

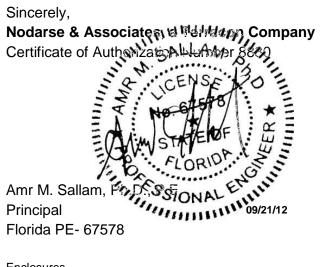
Re: Geotechnical Engineering Report Allison Oaks Pump Station No. F3215 Winter Park, Florida Terracon Project Number: AK127001

Dear Mr. Nazario:

Nodarse & Associates, a Terracon Company (Terracon) has completed the geotechnical engineering services for the above referenced project. This study was performed in general accordance with our proposal number PH1120210 dated May 2, 2012.

This report presents the findings of the subsurface exploration and provides geotechnical recommendations concerning earthwork and the design and construction of the proposed wet well pump station.

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report, or if we may be of further service, please contact us.



Jay W. Casper, P.E. Senior Associate Florida PE - 36330

Enclosures cc: 1 – Client (PDF) 1 – File

Nodarse & Associates, a Terracon Company 1675 Lee Road Winter Park, Florida 32789 P [407] 740 6110 F [407] 740 6112 terracon.com

EXECL	JTIVE S	SUMMARY	i
1.0	INTRO	DUCTION	1
	2.1	Project Description	1
	2.2	Site Location and Description	2
3.0	SUBSL	JRFACE CONDITIONS	2
	3.1	USDA Soil Survey	2
	3.2	Typical Profile	2
		Groundwater	
4.0	RECO	MMENDATIONS FOR DESIGN AND CONSTRUCTION	4
	4.1	Geotechnical Considerations	4
		4.1.1 Pump Station:	4
		4.1.2 Pipelines:	6
		4.1.4 General Site Preparation	
		4.1.5 Temporary Dewatering:	
5.0	GENE	RAL COMMENTS	7

APPENDIX A – FIELD EXPLORATION

Exhibit A-1	Site Location Map
Exhibit A-2	Soil Survey Map
Exhibit A-3	Soil Survey Descriptions
Exhibit A-4	Boring Location Plan
Exhibit A-5	Field Exploration Description
Exhibit A-6 to A-9	Boring Logs

APPENDIX B – SUPPORTING INFORMATION

APPENDIX C – SUPPORTING DOCUMENTS

Exhibit C-1	General Notes
Exhibit C-2	Unified Soil Classification System

APPENDIX D – SUSTAINABILITY CONSIDERATIONS

Exhibits D-1 to D-3 Sustainability Considerations



EXECUTIVE SUMMARY

A geotechnical investigation has been performed for the proposed Allison Oaks Pump Station planned at 3120 Patel Drive in Winter Park, Orange County, Florida. Three (3) borings, designated PB-1, PB-2, and TB-1 have been performed to depths of between 15 and 50 feet below the existing ground surface within the pump station areas. This report specifically addresses the recommendations for the proposed pump station wet well, manhole, and pipelines.

Based on the information obtained from our geotechnical exploration, it appears that the subsoil and groundwater conditions at the site are suitable for the proposed developed and construction. The following geotechnical considerations were identified:

- Temporary dewatering will be required for construction of the pump station. Dewatering the pump station area will require the use of a properly designed well point system. The dewatering system should not be turned off until the pump station has enough dead weight to counteract an uplift force calculated based on a head of water measured from the base of the pump station to the estimated Seasonal High Water Level (SHWL).
- Our borings did not encounter unsuitable soils such as muck, clay, high silts, and debris, which might cause problems during construction. However, if encountered, unsuitable soils should be completely removed to a minimum depth of 18 inches below the pump station pipelines bottom, replaced with well-draining granular sands with a fines content of less than 5 percent or less passing the No. 200 U.S. Standard sieve by weight, and compacted to a firm and unyielding state.
- The proposed structure may be supported on shallow footings bearing on the existing site soil only if the proper site preparations are following according to the appropriate sections of this report.
- On-site native soils typically appear suitable for use as general engineered fill.

This summary should be used in conjunction with the entire report for design purposes. It should be recognized that details were not included or fully developed in this section, and the report must be read in its entirety for a comprehensive understanding of the items contained herein. The section titled **GENERAL COMMENTS** should be read for an understanding of the report limitations.

GEOTECHNICAL ENGINEERING REPORT ALLISON OAKS PUMP STATION NO. F3125 WINTER PARK, FLORIDA Terracon Project No. AK127001 September 21, 2012

1.0 INTRODUCTION

A geotechnical engineering report has been prepared for the proposed Allison Oaks Pump Station which will be located at 3120 Patel Drive in Winter Park, Orange County, Florida as shown on the Topographic Vicinity Map included as Exhibit A-1 in Appendix A. Three (3) borings, designated PB-1, PB-2, and TB-1 have been performed to depths of between 15 and 50 feet below the existing ground surface in the proposed pump station and manhole area. Logs of the borings along with a site location plan, geologic map and boring location plans are included in Appendix A of this report.

The purpose of the geotechnical services was to provide information and geotechnical engineering recommendations relative to the proposed pump station wet well, gravity pipeline, and a concrete drive way. The followings will be provided:

- Field exploration method
- Subsurface soil and groundwater conditions
- Presentation of field and laboratory information in graphical format
- Recommendations for general earthwork
- Recommendations for pump station design and construction
- Recommendations for gravity pipe line earthwork

2.0 **PROJECT INFORMATION**

2.1 **Project Description**

Item	Description					
Site layout	See Appendix A, Exhibit A-4: Boring Location Plan					
Construction	One wet well to a depth of about 14 feet below existing grade and 6 feet in diameter with associated pipelines and man holes.					
Grading	Fill – fine grading, estimated at up to approximately 1 foot.					
Cut and fill slopes	Excavation per OSHA requirements or a license professional engineer for braced excavations.					



2.2 Site Location and Description

Item	Description
Location	The project will be located at 3120 Patel Drive in Winter Park, Orange County, Florida
Existing improvements	No existing structures on site. A previous structure on site has been removed.
Current ground cover	Grass covered with limited trees.
Existing topography	The USGS topographic quadrangle map "Orlando East, Florida" depicts the developed topography as nearly level, with original ground surface elevations ranging from about elevation +65 feet to +70 feet referencing the National Geodetic Vertical Datum of 1929 (NGVD29).

3.0 SUBSURFACE CONDITIONS

3.1 USDA Soil Survey

The Soil Survey of Orange County, Florida, as prepared by the United States Department of Agriculture (USDA), Soil Conservation Service (SCS; later renamed the Natural Resource Conservation Service - NRCS), dated October 1981, identifies the soil types at the project site as Zofl-Urban land complex (55). It should be noted that the Soil Survey is not intended as a substitute for site-specific geotechnical exploration; rather it is a useful tool in planning a project scope in that it provides information on soil types likely to be encountered. A copy of the pertinent section of the Soil Survey map is included as Exhibit A-2 in Appendix A. Descriptions of soil map units are included in Appendix A as Exhibit A-3.

3.2 Typical Profile

Based on the results of the borings, subsurface conditions on the project site can be generalized as follows:

Stratum	Approximate Depth to Bottom of Stratum (feet)	Material Description	Consistency/ Density
1	8	Fine sand to fine sand with silt (SP/SP-SM)	Very loose to loose



Stratum	Approximate Depth to Bottom of Stratum (feet)	Material Description	Consistency/ Density
2	8 to 38	Fine sand with silt to silty fine sand (SP/SP-SM)	Loose to medium dense
3	38 to 50	Fine sand (SP)	Medium dense to dense

Conditions encountered at each boring location are indicated on the individual boring logs. Stratification boundaries on the boring logs represent the approximate location of changes in soil types; in-situ, the transition between materials may be gradual. Details for each of the borings can be found on the boring logs in Appendix A of this report. Descriptions of our field exploration are included as Exhibit A-5 in Appendix A. Descriptions of our laboratory testing procedures are included as Exhibit B-1 in Appendix B.

3.3 Groundwater

The boreholes were observed during drilling for the presence and level of groundwater. Groundwater was observed in the borings at a depth of 10 feet below existing grade. It should be recognized that fluctuations of the groundwater table will occur due to seasonal variations in the amount of rainfall, runoff and other factors not evident at the time the boring was performed. Therefore, groundwater levels during construction or at other times in the future may be higher or lower than the levels indicated on the boring logs. The estimated seasonal high groundwater tables are included in the following table and on the boring logs.

Boring #	Approximate depth to encountered water table (feet)	Approximate depth to estimated seasonal high groundwater table (feet)
PB-1	10	8
PB-2	10	8
TB-1	10	8

Estimates of the seasonal high water table presented in this report are based on and limited by the data collected during our geotechnical exploration, and the referenced published documents. Estimates of the seasonal high assume normal precipitation volumes and distribution. These seasonal water table estimates do not represent the temporary rise in water table that occurs immediately following a storm event, including adjacent to other stormwater management facilities. This is different from static groundwater levels in wet ponds and/or drainage canals which can affect the design water levels of new, nearby ponds. The seasonal high water table may be affected by extreme weather changes, localized or regional flooding,



karst activity, future grading, drainage improvements, or other construction that may occur on our around the site following the date of this report.

4.0 **RECOMMENDATIONS FOR DESIGN AND CONSTRUCTION**

4.1 Geotechnical Considerations

The following conclusions and recommendations are based on the project characteristics previously described, the data obtained in our field exploration and our experience with similar subsurface conditions and construction types. If the proposed pump station location is significantly different from that previously described, or if subsurface conditions different from those disclosed by the borings are encountered during construction, we should be notified immediately so that we might review and modify, if necessary, the following recommendations in regards to such changes. The general guidelines included in this report are not intended to supersede more stringent requirements which may be mandated by County specifications.

4.1.1 Pump Station: Boring TB-1 was performed near the approximate location of the proposed pump station wet well as indicated by provided site plans. Groundwater was encountered in the boring at a depth of about 10 feet below existing grade. Based on the provided plans, the anticipated depth of the proposed pump station wet well is to be about 14 feet below existing grade.

- Dewatering will be required for construction of the pump station. Dewatering the pump station area will require the use of a properly designed well point system. Other dewatering systems utilizing sumps within shored or braced excavations may also be feasible. However, design of shoring/sump systems should be carefully evaluated with regard to blow outs of the excavation bottom due to unbalanced hydrostatic conditions. The Contractor should be allowed to review the soil stratification to determine the most feasible dewatering system for the pump station area. Dewatering should be performed gradually and slowly in order to reduce the effect of the sudden additional effective stress increase on the subsoil below close-by housed or roadways.
- All excavation should be performed in accordance with appropriate Occupational Safety and Health Administration (OSHA) standards. These standards typically include side slopes for temporary excavation no steeper than 1.5 horizontal to 1 vertical (1.5H: 1V) to provide adequate worker safety.
- If these side slopes cannot be maintained or are not desired due to other considerations, a properly designed and braced excavation or sheet piling would be required. All shoring



and bracing systems or sheet piling should be designed and reviewed by an experienced professional engineer registered in the State of Florida.

• Although not encountered, it is important to note that soils with high fines content (clay, silts, ect.) or unsuitable material (organics, muck, debris, ect.) should be removed to a minimum depth of 12 inches below the pump station bottom, to provide a stable construction platform, and replaced with well-draining granular sands with fines contents of 5 percent of less passing the No. 200 U.S. Standard sieve by weight. The soils below the base of the pump station should be compacted to a firm and unyielding state.

After the subgrade soils have been prepared as recommended above, the pump station may be supported on a monolithic slab or spread footing. The foundations can utilize a maximum net soil bearing pressure of 2,000 pounds per square foot.

- Compaction of backfilled soils around the pump station should be accomplished in lift thicknesses no greater than 8 inches. The fill material should consist of relatively clean granular sands with no more than 5 percent passing the No. 200 U.S. standard sieve by weight.
- Compaction can likely be accomplished in these areas with a small plate or hand guided drum type vibratory compactor and loose lift thicknesses should be limited to 8 inches. At least one (1) density test should be performed on each lift to verify that the soil has been compacted to at least 95 percent of its modified Proctor maximum dry density (ASTM D-1557).
- If compaction difficulties arise during construction, the geotechnical engineer should be consulted to provide further recommendations.
- The construction should also be sequenced so that a dewatering system, if necessary, is not turned off until the pump station has enough weight to counteract an uplift force equivalent to the amount of water displaced. It may also be prudent to place additional concrete in the structure foundation to provide ballast against such an uplift force. This uplift force should account for the head difference from the bottom elevation of the foundation to the seasonal high groundwater level or the groundwater level at the time of construction, whichever is shallower, plus any possible flooding conditions that may occur at the project site.
- For calculations of resistance to the uplift force, 50 pounds per cubic foot may be used for the buoyant unit weight of the soil. The buoyant weight of the concrete and overlying soils should be used in calculating the necessary amount of ballast required.



4.1.2 Pipelines: Regarding the pipe subgrade soils and backfill soils we offer the following recommendations:

- The bedding soil beneath the pipe should be properly shaped to completely support the pipe section and areas should be excavated to accommodate any bells or other raised portions of the pipe to help avoid point loading conditions.
- Once the pipe has been laid in the excavation trench and approved, backfill should be carefully deposited and compacted to the centerline of the pipe on both sides. All fill should be inorganic, non-plastic, granular soils (clean sands). The near surficial native site soils appear to meet backfill requirements.
- Compaction of backfilled soils above the centerline of the pipe to the proposed final grade should be accomplished in lift thicknesses no thicker than 12 inches.
- At least one (1) density per lift should be performed to verify that the soil has been compacted to 95 percent of the material's maximum modified Proctor dry density (ASTM D 1557).
- If compaction difficulties arise during construction, the Geotechnical Engineer should be consulted to provide further recommendations.

4.1.4 General Site Preparation: The following general procedures are recommended for site preparation:

- All excavations required should be performed in accordance with appropriate Occupational Safety and Health Administration (OSHA) standards. These standards typically include side slopes for temporary excavations not steeper than 1.5 Horizontal to 1 Vertical (1.5H:1V) to provide for adequate worker safety.
- If these side slopes cannot be maintained or are not desired due to other considerations, a properly designed braced excavation, trench shield, or sheet piling would be required for stable excavations. All shields, shoring and bracing systems, or sheet piling should be designed and reviewed by an experienced Professional Engineer registered in the State of Florida. Adjacent traffic loads and induced vibrations, among other factors, should be included in the design of these stabilization systems.



4.1.5 Temporary Dewatering: Groundwater was observed at a depth of about 10 feet at our boring locations at the time of our exploration. The seasonal high groundwater level is anticipated to be at a depth of about 8 feet below existing grades. Based on this information and the proposed embedment depths of the pump station, dewatering will be required to facilitate construction, backfill and compaction in the dry. Regarding dewatering, we offer the following recommendations:

- Dewatering operations at this site for the proposed pump station should be accomplished with a properly designed well point system dewatering system operating outside the excavation limits.
- The dewatering system should be adequate to lower groundwater levels to at least 2 feet below the lowest compaction surface.
- Other dewatering systems utilizing sumps within shored or braced excavations may also be feasible. However, design of shoring/sump systems should be carefully evaluated with regard to blow outs of the excavation bottom due to unbalanced hydrostatic conditions. The Contractor should be allowed to review the soil stratification to determine the most feasible dewatering system for the pump station area.

The construction should be sequenced so that the dewatering system is not turned off until the pump station has enough weight placed over it to counteract an uplift force equivalent to the height of standing water above the base of the pump station. The resisting weight of soil over the pump station should be calculated using the buoyant unit weight of the soil.

5.0 GENERAL COMMENTS

Terracon should be retained to review the final design plans and specifications so comments can be made regarding interpretation and implementation of our geotechnical recommendations in the design and specifications. Terracon also should be retained to provide observation and testing services during grading, excavation, foundation construction and other earth-related construction phases of the project.

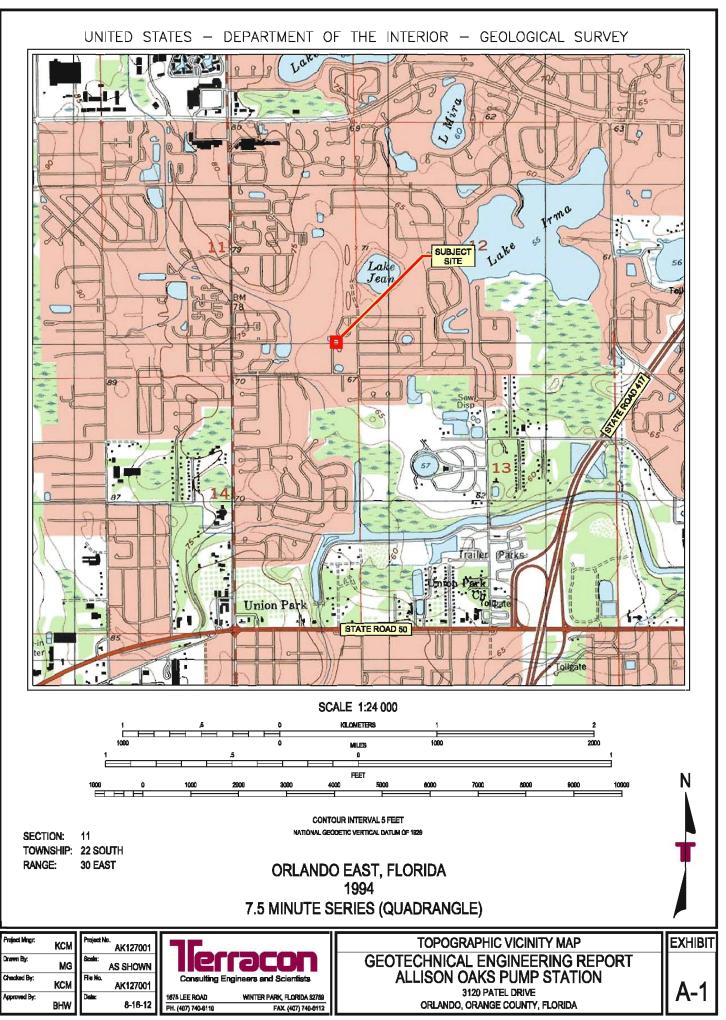
The analysis and recommendations presented in this report are based upon the data obtained from the borings performed at the indicated locations and from other information discussed in this report. This report does not reflect variations that may occur between borings, across the site, or due to the modifying effects of construction or weather. The nature and extent of such variations may not become evident until during or after construction. If variations appear, we should be immediately notified so that further evaluation and supplemental recommendations can be provided.



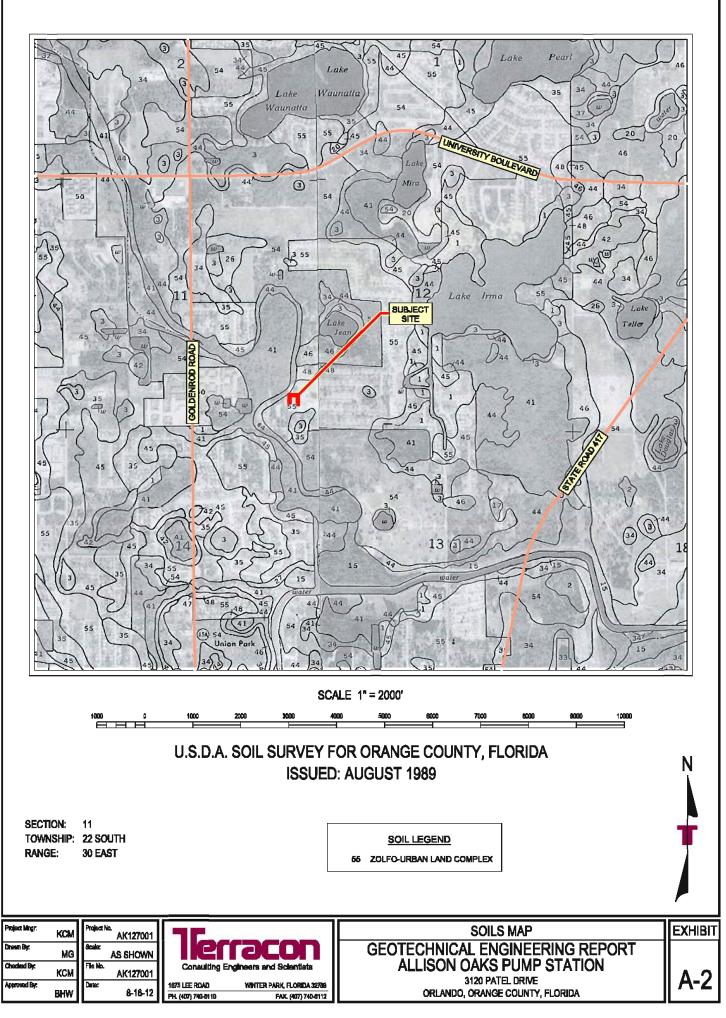
The scope of services for this project does not include either specifically or by implication any environmental or biological (e.g., mold, fungi, bacteria) assessment of the site or identification or prevention of pollutants, hazardous materials or conditions. If the owner is concerned about the potential for such contamination or pollution, other studies should be undertaken.

This report has been prepared for the exclusive use of our client for specific application to the project discussed and has been prepared in accordance with generally accepted geotechnical engineering practices. No warranties, either express or implied, are intended or made. Site safety, excavation support, and dewatering requirements are the responsibility of others. In the event that changes in the nature, design, or location of the project as outlined in this report are planned, the conclusions and recommendations contained in this report shall not be considered valid unless Terracon reviews the changes and either verifies or modifies the conclusions of this report in writing.

APPENDIX A FIELD EXPLORATION



ojectr\2012\4K127001\PROJECT DOCIMENTS (Reports-Latines-Dwifts to Chemic)\Cod(4K127001-Eathble-A-1.4mg





Soil Survey Descriptions

<u>55 – Zolfo-Urban land complex.</u> This complex consists of areas of Zolfo soil that is nearly level and somewhat poorly drained and areas of Urban land. It is typically found in broad, slightly higher positions adjacent to the flatwoods. Drainage systems have been established in most areas. The depth to the seasonal high water table is dependent upon the functioning of the drainage system. In undrained areas, this soil map unit has an apparent seasonal high water table between depths of 24 and 40 inches (2.0 and 3.3 feet) for 2 to 6 months and at a depth of 10 to 24 inches (0.8 to 2.0 feet) during periods of high rainfall. It recedes to a depth of more than 60 inches (5.0 feet) during extended dry periods. Zolfo soil is predominantly sandy throughout the defined profile of 80 inches (6.7 feet). The areas of Urban land have been covered or altered such that the natural soil profile is no longer observable.





Field Exploration Description

The boring locations were laid out at the project site by Terracon personnel. The locations indicated on the attached diagram are approximate and were measured by pacing distances and estimating right angles, across vegetated/wooded terrain. The locations of the borings should be considered accurate only to the degree implied by the means and methods used to define them.

The SPT soil borings were drilled with an truck-mounted, rotary drilling rig equipped with a rope an automatic hammer. The boreholes were advanced with a cutting head and stabilized with the use of bentonite (drillers' mud). Soil samples were obtained by the split spoon sampling procedure in general accordance with the Standard Penetration Test (SPT) procedure. In the split spoon sampling procedure, the number of blows required to advance the sampling spoon the last 12 inches of an 18-inch penetration or the middle 12 inches of a 24-inch penetration by means of a 140-pound hammer with a free fall of 30 inches, is the standard penetration resistance value (N). This value is used to estimate the in-situ relative density of cohesionless soils and the consistency of cohesive soils. The sampling depths and penetration distance, plus the standard penetration resistance values, are shown on the boring logs.

Portions of the samples from the borings were sealed in glass jars to reduce moisture loss, and then the jars were taken to our laboratory for further observation and classification. Upon completion, the boreholes were backfilled with the site soil.

Field logs of each boring were prepared by the drill crew. These logs included visual classifications of the materials encountered during drilling as well as the driller's interpretation of the subsurface conditions between samples. The boring logs included with this report represent an interpretation of the field logs and include modifications based on laboratory observation of the samples.

A CME automatic SPT hammer was used to advance the split-barrel sampler in the borings performed on this site. A significantly greater efficiency is achieved with the automatic hammer compared to the conventional safety hammer operated with a cathead and rope. This higher efficiency has an appreciable effect on the SPT-N value. The effect of the automatic hammer's efficiency has been considered in the interpretation and analysis of the subsurface information for this report.

BORING LOG NO. PB-1 Page 1 of 1								
PROJECT: Allison Oaks Pump Station No. F3215 - Wet Well		CLIENT: Orang Orlan	ge County P Ido, Florida	ublic	Util	lities		
SITE: 3120 Patel Drive Winter Park, Orange County, F								
UCATION Exhibit A-4			DEPTH (ft)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	PERCENT FINES
FINE SAND WITH SILT (SP-SM), gray				-				
, J			5			2-2-3-2 N=5		
8.0 SILTY FINE SAND (SM), tan, loose				_		2-2-3-3 N=5 3-3-2-2	21	16
						N=5		
			15	_		5-4-5 N=9		
				_				
Stratification lines are approximate. In-situ, the transition may be			25	_				
Stratification lines are approximate. In-situ, the transition may be	gradual.		Hammer Type: A	Automatic	;			
Rotary Drilling Cutting Head Abandonment Method:	See Exhibit A-5 for description of the sector of the sector of the sector procedures and additional See Appendix C for explanation of the sector of the sect	iption of laboratory I data, (if any).	Notes:					
Borings backfilled with soil cuttings upon completion.	abbreviations.	-						
WATER LEVEL OBSERVATIONS Water Initially Encountered			Boring Started: 8/8/ Drill Rig: Truck	2012		Boring Completed Driller: Travis	8/8/2012	2
Estimated Seasonal High Water Level @ 8'	1675 Le Winter Pa	e Road	Project No.: AK127	001		Exhibit A-6		

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. SMART LOG-DEPTH TO BOTTOM OF PAGE AK127001-ALLISON OAKS.GFJ TERRACON2012.GDT 8/28/12

	E	BORING LC	OG NO. PB-	-2			Page	e 1 of 1	1
PR	OJECT: Allison Oaks Pump Station No. F3215 - Wet Well		CLIENT: Orang Orlan	ge County Pu Ido, Florida	ıblic	Util			
SIT	E: 3120 Patel Drive Winter Park, Orange County, I	Florida	SPT Borings						-
GRAPHIC LOG	LOCATION Exhibit A-4			DEPTH (ft)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	PERCENT FINES
	FINE SAND (SP), light brown to grayish-brown,	very loose to mediun	n dense	-	-				
				-	-			5	5
				5 -	-		2-1-1-2 N=2		
				-	_		1-1-2-4 N=3		
				- 10-			6-5-6-4 N=11		
				-	-				
	13.5 SILTY FINE SAND (SM), brown, loose				-		2-2-5		
	15.0 Boring Terminated at 15 Feet			15-			N=7		
				-	-				
				-	-				
				20-	-				
				-	-				
				- 25-	-				
	Stratification lines are approximate. In-situ, the transition may be	e gradual.		Hammer Type: Au	tomatic				<u> </u>
	ement Method: Iry Drilling Cutting Head	See Exhibit A-5 for descri	ption of field procedures	Notes:					
	onment Method: ngs backfilled with soil cuttings upon completion.	See Appendix B for descr procedures and additional See Appendix C for expla abbreviations.							
	WATER LEVEL OBSERVATIONS		-				I		
\Box	Water Initially Encountered		ODARSE	Boring Started: 8/8/20)12		Boring Completed:	8/8/2012	2
		^]	Erracon COMPANY	Drill Rig: Truck			Driller: Travis		
	Estimated Seasonal High Water Level @ 8'		ee Road ark, Florida	Project No.: AK12700)1		Exhibit A-7		

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. SMART LOG-DEPTH TO BOTTOM OF PAGE AK127001-ALLISON OAKS.GFJ TERRACON2012.GDT 8/28/12

٢

	BORING LOG NO. TB-1 Page 1 of 2										
PR	PROJECT: Allison Oaks Pump Station CLIENT: 0				nge County Public Utilities ando, Florida						
SIT	E: 3120 Patel Drive Winter Park, Orange County, F	Florida	SPT Borings								
GRAPHIC LOG	LOCATION Exhibit A-4				DEPTH (ft)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	PERCENT FINES	
	DEPTH FINE SAND WITH SILT (SP-SM), grayish-brow	n									
	4.0				_						
	FINE SAND (SP), light brown, loose				- 5			2-2-2-2 N=4			
	8.0				_			2-2-3-3 N=5			
	FINE SAND WITH SILT (SP-SM), tan to light br	own, loose to mediur	n dense		_ 10—	∇		3-2-2-2 N=4			
					-						
					- 15-			1-2-2 N=4	27	9	
					_						
					_ 20—	-		3-4-3 N=7			
					_	-					
					_ 25—			5-5-5 N=10			
	Stratification lines are approximate. In-situ, the transition may be	aradual		Hammer T	vpe: Aut	omatic					
		-			, po. 7 dt						
Advancement Method: See Exhibit A-5 for description of field procedures Rotary Drilling Cutting Head See Appendix B for description of laboratory				Notes:							
Abando Borir	onment Method: ngs backfilled with soil cuttings upon completion.	see Appendix B for descr procedures and additiona See Appendix C for expla abbreviations.	l data, (if any).								
	WATER LEVEL OBSERVATIONS	N 1		Boring Starte	ed: 8/8/20	12		Boring Completed	8/8/2012	2	
	Water Initially Encountered			Drill Rig: Truc	ck			Driller: Travis			
	Estimated Seasonal High Water Level @ 8'		ee Road irk, Florida	Project No.: A	AK12700	1		Exhibit A-8			

BORING LOG NO. TB-1 Page 2 of 2											
PR	OJECT: Allison Oaks Pump Station No. F3215 - Wet Well		CLIENT: Oran Orlan	ge County Pu ido, Florida	blic	Util					
SIT	E: 3120 Patel Drive Winter Park, Orange County, F	Florida	SPT Borings								
GRAPHIC LOG	LOCATION Exhibit A-4			DEPTH (ft)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	PERCENT FINES		
	DEPTH FINE SAND WITH SILT (SP-SM), tan to light brown, loose to medium dense (continued)										
				-							
		AND WITH SILT (SP-SM), tan to light brown, loose to medium dense (continued)				5-4-5 N=9	27	9			
				-	-						
							7-7-8 N=15				
	38.5				-						
FINE SAND (SP), light brown, medium dense to dense				-			6-8-9 N=17				
				40- - -	-						
				45-	-		13-17-21 N=38				
				-	-						
	50.0			-			10-14-19 N=33				
	Boring Terminated at 50 Feet			50- _ _	-						
	Stratification lines are approximate. In-situ, the transition may be	gradual.		Hammer Type: Au	tomatic						
Rota	zement Method: ny Drilling Cutting Head onment Method: ngs backfilled with soil cuttings upon completion.	See Exhibit A-5 for descrip See Appendix B for descri procedures and additional See Appendix C for explar abbreviations.	ption of laboratory data, (if any).	Notes:							
	WATER LEVEL OBSERVATIONS		Boring Started: 8/8/20	Boring Started: 8/8/2012 Boring Completed: 8/8/2012							
Water Initially Encountered			DOARSE Terracon communy Drill Rig: Truck				Driller: Travis				
Estimated Seasonal High Water Level @ 8' Winter Park, Florida		e Road	Project No.: AK127001 Exhibit A-9								

THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT. SMART LOG-DEPTH TO BOTTOM OF PAGE AK127001-ALLISON OAKS.GFJ TERRACON2012.GDT 8/28/12

APPENDIX B – LABORATORY TESTING



Laboratory Testing

During the field exploration, a portion of each recovered sample was sealed in a glass jar and transported to our laboratory for further visual observation and laboratory testing. Selected samples retrieved from the borings were tested for moisture (water) content, fines content (soil passing a US standard #200 sieve). Those results are included in this report and on the respective boring logs, except for permeability. The visual-manual classifications were modified as appropriate based upon the laboratory testing results.

The soil samples were classified in general accordance with the appended General Notes and the Unified Soil Classification System based on the material's texture and plasticity. The estimated group symbol for the Unified Soil Classification System is shown on the boring logs and a brief description of the Unified Soil Classification System is included in Appendix B. The results of our laboratory testing are presented in the Laboratory Test Results section of this report and on the corresponding borings logs.

APPENDIX C SUPPORTING DOCUMENTS

UNIFIED SOIL CLASSIFICATION SYSTEM

Criteria for Assigning Group Symbols and Group Names Using Laboratory Tests^A

Criteria for Assign	Group Symbol	Group Name ^B			
	Gravels: More than 50% of coarse fraction retained on No. 4 sieve	Clean Gravels:	$Cu \ge 4$ and $1 \le Cc \le 3^{E}$	GW	Well-graded gravel F
		Less than 5% fines ^C	$Cu < 4$ and/or $1 > Cc > 3^{E}$	GP	Poorly graded gravel F
		Gravels with Fines: More than 12% fines ^c	Fines classify as ML or MH	GM	Silty gravel F,G,H
Coarse Grained Soils: More than 50% retained			Fines classify as CL or CH	GC	Clayey gravel F,G,H
on No. 200 sieve	Sands: 50% or more of coarse fraction passes No. 4 sieve	Clean Sands: Less than 5% fines ^D	$Cu \ge 6$ and $1 \le Cc \le 3^{E}$	SW	Well-graded sand ¹
			$Cu < 6$ and/or $1 > Cc > 3^{E}$	SP	Poorly graded sand
		Sands with Fines: More than 12% fines ^D	Fines classify as ML or MH	SM	Silty sand G,H,I
			Fines classify as CL or CH	SC	Clayey sand G,H,I
	Silts and Clays: Liquid limit less than 50	Inorganic:	PI > 7 and plots on or above "A" line ^J	CL	Lean clay ^{K,L,M}
			PI < 4 or plots below "A" line ^J	ML	Silt ^{K,L,M}
		Organic:	Liquid limit - oven dried < 0.75	OL	Organic clay K,L,M,N
Fine-Grained Soils: 50% or more passes the			Liquid limit - not dried		Organic silt K,L,M,O
No. 200 sieve	Silts and Clays: Liquid limit 50 or more	Inorganic:	PI plots on or above "A" line	СН	Fat clay K,L,M
			PI plots below "A" line	MH	Elastic Silt K,L,M
		Organic:	Liquid limit - oven dried < 0.75	ОН	Organic clay K,L,M,P
			Liquid limit - not dried		Organic silt K,L,M,Q
Highly organic soils:	Primarily	PT	Peat		

^A Based on the material passing the 3-inch (75-mm) sieve

^B If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.

- ^c Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with silt, GW-GC well-graded gravel with clay, GP-GM poorly graded gravel with silt, GP-GC poorly graded gravel with clay.
- ^D Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt, SW-SC well-graded sand with clay, SP-SM poorly graded sand with clay

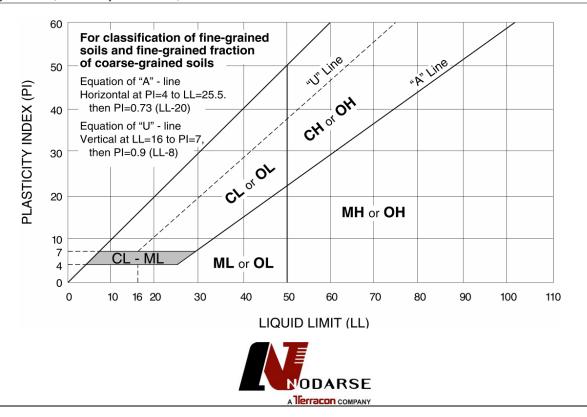
^E Cu = D₆₀/D₁₀ Cc =
$$\frac{(D_{30})^2}{D_{10} \times D_{60}}$$

 $^{\rm F}$ If soil contains \geq 15% sand, add "with sand" to group name. $^{\rm G}$ If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

- ^H If fines are organic, add "with organic fines" to group name.
- If soil contains \geq 15% gravel, add "with gravel" to group name.
- ^J If Atterberg limits plot in shaded area, soil is a CL-ML, silty clay.
- ^K If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel," whichever is predominant.

Soil Classification

- ^L If soil contains ≥ 30% plus No. 200 predominantly sand, add "sandy" to group name.
- ^M If soil contains \geq 30% plus No. 200, predominantly gravel, add "gravelly" to group name.
- ^N $PI \ge 4$ and plots on or above "A" line.
- ^o PI < 4 or plots below "A" line.
- ^P PI plots on or above "A" line.
- ^Q PI plots below "A" line.



APPENDIX D SUSTAINABILITY CONSIDERATIONS

SUSTAINABILITY CONSIDERATIONS

LEED Sustainable Sites (SS)

SS Prerequisite 1 – Construction Activity Pollution Prevention

The intent is to reduce pollution from construction activities by controlling soil erosion, waterway sedimentation and airborne dust generation. Terracon can assist in developing site specific Storm Water Management Plans (SWMP's) in addition to providing observation services for the duration of the project for conformance to the SWMP's.

SS Credit 5.1 - Site Development – Protect or Restore Habitat

The intent is to conserve existing natural areas and restoring damaged areas to provide habitat and promote biodiversity. Terracon can provide restoration recommendations such as design of mechanically stabilized earth vegetative faced retained slopes, stream mitigation, etc.

SS Credit 6.1 and Credit 6.1 – Storm Water Design – Quantity Control and Quality Control

Sustainable storm water design limits disruption of natural hydrology by reducing impervious cover, increasing on-site infiltration, and managing storm water runoff. Terracon can provide design recommendations for porous pavement systems and infiltration basins to assist in maintaining pre-development peak discharge rates of design storms without compromising the structural capacity of the pavement or surrounding improvements. A pervious pavement system is a pavement that is sufficiently porous to allow the infiltration of water into a sub-drainage system or open-graded aggregate base reservoir below paved areas. The collected water is allowed to infiltrate through a filter fabric into the underlying subgrade soils or the water is collected and discharged to a suitable outlet.

LEED Energy and Atmosphere (EA)

EA Credit 2 – On-site Renewable Energy

The intent is to provide on-site renewable energy. Self supply renewable energy potentials Include horizontal and vertical loop fields. Terracon can provide thermal resistivity testing for horizontal loop fields or trial testing for vertical geothermal wells.

LEED Materials and Resources (MR)

MR Credit 2 – Construction Waste Management

The intent is to divert construction and demolition debris from disposal in landfills and incineration facilities.

<u>Reuse of On-Site Building Materials or Construction Debris:</u> Reusing inorganic building materials derived from foundation demolition or construction debris as processed fill material is acceptable provided the materials are crushed to a well-graded homogenous mixture and free of wood and other deleterious debris. Crushed concrete foundations, flatwork and brick may be incorporated into structural compacted fill in approved areas.

Maximum size of crushed material should be no greater than 3 inches. Use of fill materials will depend upon the source of the recycled material and the intended use. Materials such as wood and metal should be properly disposed off-site. *Caution should be used when specifying painted recycled materials. In some states, the paint would need to be analyzed to evaluate if it is lead-based. The text above may need to be edited to say "uncoated" building materials*

<u>Use of On-site Crushed Asphaltic Cement Concrete (ACC) Pavement for Engineered Fill:</u> ACC pavement, and the underlying base rock can be used as engineered fill as long as it is properly processed. It is important that the recycled ACC pavement be blended with another material, such as soil, sand, and/or gravel, to fill voids. This material should be well graded and have a maximum size, in any dimension, of 6-inches. This may necessitate the use of on-site screening of the materials and processing the oversized portion through a crusher such that the maximum size of the well graded blend would be 6-inches.

Recycled ACC pavement should be limited to a maximum of 50% of the fill material being placed in any lift. This material should be used deep within the fill or in non-structural areas such that it does not underlie future excavations being made for footings, utilities, etc.

MR Credit 4 – Recycled Content

<u>Flowable Fill:</u> Consider using flowable fill for trench backfill. The flowable fill should be comprised of waste materials such as waste limestone screenings as the bulk-filler and fly-ash for the cementitious component.

<u>ACC Pavement:</u> ACC Pavement produced in the Central Florida area typically includes 20 percent recycled asphalt pavement (RAP) and 4 percent recycled asphalt shingles resulting in a product that contains 24% recycled material.

Limestone Screenings (Waste Lime): Limestone screenings are a waste product produced by many Central Florida Quarries. This material is usually wasted in the quarries if it does not possess enough calcium content to be suitable for ag-lime applications and also because there is more product produced than demand can satisfy. As a result, this material is abandoned on-site as a waste product. This material typically is well graded crushed aggregate material with an approximate top size of ¼-inch. This material can be used as engineered fill material in structural and non-structural areas of the project. The limestone screenings can be used for the low volume change zones as a suitable replacement for shrink/swell prone soils.

<u>Supplementary Cementitious Materials (SCM's):</u> Consider using SCM's that are recycled from other operations, such as fly ash, in concrete mixes.

<u>Soil Subgrade Stabilization:</u> Consider using Fly-Ash or Code-L (a waste by-product produced when making cement) to stabilize or otherwise improve the soil subgrade.

MR Credit 5: Regional Materials

Using regional materials is intended to increase demand for building materials and products that are extracted and manufactured within the region. Regional materials also reduce environmental impacts caused by transportation.

<u>Asphaltic Cement Pavement (ACC)</u>: ACC pavement is typically produced locally. Asphalt and aggregates are typically derived locally. Oils may or may not be derived locally.

<u>Portland Cement Concrete (PCC):</u> PCC is typically derived locally including sand, gravel, water, and cement. Additives may or may not be locally derived.

<u>Aggregates for Base and Backfill:</u> Coarse and fine aggregates are typically derived locally from quarrying operations or from dredging operations.

National Pollutant Discharge Elimination System Groundwater Testing and Database Search

Allison Oaks Pump Station No. F3215 3120 Patel Drive, Winter Park Orange County, Florida

October 4, 2012 Nodarse/Terracon Project No. AK127001

Prepared for: Orange County Public Utilities-Engineering Division Orlando, Florida

> Prepared by: Nodarse & Associates, Inc. A Terracon Company Winter Park, Florida 32789

Offices Nationwide Employee-Owned nodarse.com terracon.com





October 4, 2012

Orange County Utilities Department Engineering Division 9150 Curry Ford Road Orlando, Florida 32825

- Attn: Mr. Heriberto Collado-Lopez, P.E. Phone: 407-254-9900 Fax: 407-254-9999
- Re: Groundwater Sampling/Testing National Pollutant Discharge Elimination System (NPDES) Parameters Allison Oaks Pump Station No. F3215 3120 Patel Drive, Winter Park, Orange County, Florida Nodarse/Terracon Project No. AK127001

Dear Mr. Collado:

In accordance with your request and authorization, Nodarse & Associates, Inc., a Terracon Company (Nodarse/Terracon), has completed National Pollutant Discharge Elimination System (NPDES) groundwater quality sampling and testing services at the above referenced location in accordance with our proposal number PH1120210 dated May 2, 2012, and Orange County Purchase Order #C11903A012, dated July 10, 2012.

A review of the Florida Department of Environmental Protection's (FDEP's) Contamination Locator Database website did not reveal the presence of any identified contaminated site within 1,000 feet of the project site.

On September 19, 2012, a temporary monitor well (TMW-3) was installed by direct-push Geoprobe drilling method to a depth of 13 feet below land surface (BLS). The depth to the shallow water table was measured at 6.7 feet BLS. On September 20, 2012, after well purging and stabilization of groundwater field parameters, Nodarse/Terracon collected one representative groundwater sample (PS# FS3215) for laboratory testing. The groundwater sample was delivered to Southern Research Laboratories, Inc. (SRL) of Orlando, Florida (Florida Department of Health #E83484) for analysis of NPDES parameters.

As shown in Table 1, the reported concentration of one parameter, total copper (detected at 4.58 micrograms per liter [μ g/l]), exceeded the Chapter 62-621.300 (2), Florida Administrative Code, listed screening value (LSV) of 2.9 μ g/l. If the dewatering effluent will be discharged onto the project site or sanitary sewer, then re-sampling of the temporary monitoring well for total copper may not to be warranted. Otherwise, re-sampling is recommended for total copper only. The remaining parameters analyzed did not report exceedances above their respective LSVs.



Nodarse & Associates, a Terracon Company 1675 Lee Road Winter Park, Florida 32789 P [407] 740 6110 F [407] 740 6112 terracon.com



A copy of the laboratory analytical report, the groundwater sampling log, instrument calibration sheet, the monitoring well details and a site photograph are included in Appendix A.

Nodarse/Terracon appreciates the opportunity to have assisted with these services. If you should have any questions or comments, please feel free to contact us.

Sincerely, Nodarse & Associates, Inc., a Terracon Company

Project Environmental Scientist



N:\Projects\2012\AK127001\PROJECT DOCUMENTS (Reports-Letters-Drafts to Clients)\NPDES Allison Oaks\AK127001 Final NPDES Report doc

TABLE

TABLE 1

GROUNDWATER ANALYTICAL SUMMARY FINAL RESULTS OF NPDES CONCENTRATIONS ALLISON OAKS PUMP STATION #F3215 WINTER PARK, ORANGE COUNTY, FLORIDA NODARSE/TERRACON PROJECT NO. AK127001 SAMPLING DATE: SEPTEMBER 20, 2012

	Sample ID		
PARAMETER DATE SAMPLED	PS #FS3215 9/20/12	Limits*	Units
Benzene	0.50 U	1.0	μg/L
Naphthalene	0.10 U	100	μg/L
Cadmium, Total	0.306 U	9.3	μg/L
Copper, Total	4.58 i	2.9	μg/L
Lead, Total	1.60 U	30.0	μg/L
Mercury, Total	0.00195	0.012	μg/L
Zinc, Total	10.3 v	86.0	μg/L
Chromium, Hexavalent	4.2 U	11.0	μg/L
Total Organic Carbon (TOC)	6.9	10.0	mg/L
TRPH	200 U	5000.0	μg/L
pH - Field	6.44	6.0 - 8.5	μg/L
Turbidity	2.41	NA	NTU

NOTES:

Bold values represent a concentration exceeding the respective NPDES criteria

mg/L - milligrams per liter

µg/L - micrograms per liter

i - indicates value < method detection limit but > than practical quantitation limit

I - The reported concentration is between the MDL and PQL

U - not detected above method detection limit

v - Analyte was detected in both the sample and associated Lab Method Blank; laboratory contamination

* Based on the Florida Department of Environmental Protection' s Effluent Discharge

Generic Dewatering Permit Table 4 Screening Values (Doc # 62-621.300(1), eff. 2-14-2000

NS - No applicable limitation or standard referenced

NA - Not applicable

APPENDIX A

LABORATORY ANALYTICAL REPORT, GROUNDWATER SAMPLING LOGS, INSTRUMENT CALIBRATION SHEET, MONITORING WELL DETAILS AND PHOTOGRAPH



2251 Lynx Lane, Suite 1 Orlando, Florida 32804 (407) 522-7100 Fax (407) 522-7043 Toll Free 1 (888) 420-Test

Thank you **Mr. Ed Sainten** for the opportunity to be of service to you and your company; we Sincerely Appreciate Your Business. SRL certifies these **Laboratory Results** were produced in accordance with NELAC Standards. Hold times and preservation requirements were met for all analytes unless specifically noted in the report. Results relate only to the samples as received.

Client Name: Te	rracon		Date(s) Collected: 09/20/12
Contact Name: E	d Sainten		Date Received: 09/20/12
Project Name: A	llison Oak's PS #F3215		Time Received: 13:08
Project Number: AK-12-7001			Date Reported : 10/01/12
Phone Number: (407) 740-6110			Date Emailed : 10/01/12
Fax Number: (407) 740-6112			SRL Work Order # 12-09024
SRL WO #	Clients #	Matrix	Analysis Requested
12-09024-001	PS #FS3215	Liquid	EPA8260(Benz)/TOC/Cd/Cu/Pb/Zn/
			8270-SIM(PAH)Naph/FLPRO/
			LL Hg/Hexavalent Chromium
12-09024-002	Trip Blank	Liquid	EPA 8260 (Benz)



Sherri Payne Vice President & Quality Assurance Officer Southern Research Laboratories, Inc.

This report, which includes the attached Chain-of-Custody, shall not be reproduced except in full, without written approval of the laboratory.

Southern Research Laboratories, Inc.		NELAP Certified
an MBE Environmental Labo	E Environmental Laboratory FDOH Cer	
2251 Lynx Lane, Suite 1		SRL Lab Ref # : 12-09024
Orlando, Florida 32804	(407) 522-7100	Received Date : 09/20/12
Ed Sainten		Project Number/Project Name
Terracon		AK-12-7001
1675 Lee Rd.		Allison Oak's PS #F3215
Winter Park, FL 32789	(407) 740-6110	Orlando, FL

EPA Method 5030/8260B VOA {602} Compounds in Water by GC-MS

Client ID #	: PS #FS3215	Trip Blank	Method Blank			
SRL (Lab) ID#	: 12-09024-00	1 12-09024-002	MB092512			
Date Collected	: 09/20/12	09/18/12	NA			
Lab FDOII Certification #	: E83484	E83484	E83484			
Date Prepared	: 09/25/12	09/25/12	09/25/12			
Date Analyzed	: 09/25/12	09/25/12	09/25/12	MDL	PQL	CAS Number
Benzene	0.5 U	0.5 U	0.5 U	0.5	1.0	71-43-2
Units	: ug/L	ug/L	ug/L	ug/L	ug/L	
Dilution Factor (MEDF)	: 1	1	1	1	1	
Surrogate (% Rec)	:			(Surrogat	e Contro	ol Limits)
4-Bromofluorobenzene	92.5%	97.4%	95.0%		70-130	

		LCS	MS/MSD		
	% Recovery	Acceptable	Acceptable	%RPD	Acceptable
	LCS/MS/MSD	Limits	Limits	MS/MSD	Limits
Benzene	109/81/81	70-130	70-130	0.5	0-30

EPA Method 3510/8270C-SIM Polynuclear Aromatic Hydrocarbon Compounds +Naph in Water by GC-MS

Client ID #	: PS #FS3215	Method Blank				
SRL (Lab) ID#	: 12-09024-001	MB092512				
Date Collected	: 09/20/12	NΛ				
Lab FDOII Certification #	: E83484	E83484				
Date Extracted	: 09/25/12	09/25/12				
Date Analyzed	: 09/26/12	09/26/12		MDL	PQL	CAS Number
Naphthalene	0.10 U	0.10 U		0.10	0.50	91-20-3
Units	: ug/L	ug/L		ug/L	ug/L	
Dilution Factor (MEDF)	: 1	1		1	1	
Surrogate (% Rec)				(Surroga	te Contro	ol Limits)
Nitrobenzene-D5	89.2%	87.3%			60-140	
2-Fluorobiphenyl	79.2%	74.6%			60-140	
p-Terphenyl-D14	99.3%	105.2%			60-140	
	% Recovery	Acceptable	%RPD	Acceptable		
Naphthalenc	LCS/MS/MSD 83/76/82	Limits 60-140	MS/MSD 7.6	Limits 30		

Southern Research Laboratorn an MBE Environmental Labora 2251 Lynx Lane, Suite 1 Orlando, Florida 32804 Ed Sainten Terracon	,	00			FDOH SRL L Receiv	ab Ref# ed Date t Numbe	fied : E83484 # : 12-09024 : : 09/20/12 er/Project Name
1675 Lee Rd.					Allison	ı Oak's	PS #F3215
Winter Park, FL 32789	(407) 740-611	10			Orlan	do, FL	
	<u>FL-PRO (Pe</u>	etroleum Range	Organics)~{V	Water}			
Client ID # SRL (Lab) ID# Date Collected Lab FDOH Certification # Date Prepared Date Analyzed TOTAL PRO (C8-C40) Units Dilution Factor (MEDF) Surrogate (% Rec) Orthoterphenyl (OTP)	: PS #FS3215 : 12-09024-001 : 09/20/12 : E83484 : 09/26/12 : 09/27/12 0.2 U : mg/L : 1 : 86.2%	Method Blank MB092612 NA E83484 09/26/12 09/27/12 0.2 U mg/L 1 115.7%			MDL 0.2 mg/L 1 (Surrogat	PQL 0.5 mg/L 1 cc Contro 82-142	CAS Number NA
TOTAL PRO (C8-C40)	% Recovery LCS/LCSD 84/85 <u>Hexavalent Ch</u>	Acceptable Limits 55-118	% RPD LCS/LCSD 1.7 18 3500-Cr D	Acceptable Limits 0-20 in Water	c		
Client ID #	: PS #FS3215	Method Blankl	Method Blank	2			
SRL (Lab) ID#	: 12-09024-001	MB092012	MB092112				
Date Collected	: 09/20/12	NA	NA				
Lab FDOH Certification #	: E82277	E83182	E83182				
Date Prepared	: 09/21/12	09/20/12	09/21/12				
Date Analyzed	: 09/21/12	09/20/12	09/21/12				
Time Analyzed	: 10:00	22:09	9:51				
Units	<u>: mg/L</u>	mg/L	mg/L			PQL	CAS Number

 Units
 : mg/L
 mg/L
 mg/L
 MDL
 PQL
 CAS Number

 Hexavalent Chromium
 0.0042
 U
 0.0042
 U

	% Recovery LCS/MS/MSD	LCS Acceptable Limits	MS/MSD Acceptable Limits	% RPD MS/MSD	Acceptable Limits	
Hexavalent Chromium	106/92/93	85-115	85-115	2	0-13	

Southern Research Laborato an MBE Environmental Labo 2251 Lynx Lane, Suite 1 Orlando, Florida 32804		00			FDOH SRL L		
Ed Sainten Terracon 1675 Lee Rd. Winter Park, FL 32789	(407) 740-61	10			AK-12 Alliso	2-7001	r/Project Name PS #F3215
	<u>Total Organ</u>	ic Carbon by SN	<u>/18 5310B in</u>	Water			
Client ID # SRL (Lab) ID# Date Collected Lab FDOH Certification # Date Prepared Date Analyzed Dilution Factor (MEDF) Units	: PS #FS3215 : 12-09024-001 : 09/20/12 : E82277 : 09/26/12 : 09/26/12 : 1 : mg/L	Method Blank MB092612 NA E83182 09/26/12 09/26/12 1 mg/L			MDL	PQL	CAS Number
Total Organic Carbon (TOC)	6.9	0.22			0.22	1.0	ECL-0165
Total Organic Carbon (TOC)	% Recovery LCS/MS/MSD 100/103/104	Acceptable Limits 85-115	% RPD MS/MSD 0.7	Acceptable Limits 0-21			
	EPA Method 1	631 Low Lev <u>el I</u>	Mercury (Hg)	in Water			
Client ID # SRL (Lab) ID# Date Collected Lab FDOII Certification # Date Prepared Date Analyzed Units	: PS #FS3215 : 12-09024-001 : 09/20/12 : E87688 : 09/24/12 : 09/25/12 : ng/L	Method Blank MB092412 NA E87688 09/24/12 09/25/12 ng/L			MDL	PQL	CAS Number
Low Level Mcrcury (Hg)	1.95	0.183 U			0.183	0.5	7439-97-6
Low Level Mercury (Hg)	% Recovery LCS/MS/MSD 107/100/91	LCS Acceptable Limits 77-123	MS/MSD Acceptable Limits 71-125	% RPD MS/MSD 8.7	A	cceptabl Limits 0-24	e

Southern Research Laborato	ories, Inc.		NELAP Certified
an MBE Environmental Labo	FDOH Cert # : E83484		
2251 Lynx Lane, Suite 1			SRL Lab Ref # : 12-09024
Orlando, Florida 32804	(407) 522-710	00	Received Date : 09/20/12
Ed Sainten			Project Number/Project Name
Terracon			AK-12-7001
1675 Lee Rd.			Allison Oak's PS #F3215
Winter Park, FL 32789	(407) 740-61	.0	Orlando, FL
	<u>Metals (total re</u>	coverable) by EPA 200 Series	Methods
Client ID #	: PS #FS3215	Method Blank	
SRL (Lab) ID#	: 12-09024-001	MB092412	
Date Collected	: 09/20/12	NA	

Diffe Concered	. 07/20/12				
Lab FDOH Certification #	: E82277	E82277			
Date Prepared	: 09/24/12	09/24/12			
Date Analyzed	: 09/25/12	09/25/12			
Units	: ug/L	ug/L	MDL	PQL	CAS Number
Cadmium	0.306 U	0.306 U	0.306	1.00	7440-43-9
Copper	4,58 I	1.40 U	1.40	10.0	7440-50-8
Lead	1.60 U	1.60 U	1.60	10.0	7439-92-1
Zinc	10.3 V	* 7.86 I	3.00	10.0	7440-66-6

		LCS	MS/MSD		
Prep. Method EPA 3005A	% Recovery	Acceptable	Acceptable	%RPD	Acceptable
EPA 200.7	LCS/MS/MSD	Limits	Limits	MS/MSD	Limits
Cadmium	104/102/102	85-115	70-130	0.1	0-25
Copper	101/101/101	85-115	70-130	0.2	0-25
Lead	102/100/100	85-115	70-130	0.7	0-25
Zinc	99/98/97	85-115	70-130	0.7	0-25

* This compound is a common laboratory contaminant

,

Southern Research Laborato	ries, Inc.	NELAP Certified
an MBE Environmental Labor	ratory	FDOH Cert # : E83484
2251 Lynx Lane, Suite 1		SRL Lab Ref # : 12-09024
Orlando, Florida 32804	(407) 522-7100	Received Date : 09/20/12
Ed Sainten		Project Number/Project Name
Terracon		AK-12-7001
1675 Lee Rd.		Allison Oak's PS #F3215
Winter Park, FL 32789	(407) 740-6110	Orlando, FL

DATA QUALIFIER CODES

Reporting Exceptions and Qualified Data

When quality control results are outside established control limits reanalysis, including re-extraction (if applicable), is preferred. If re-analysis is not viable or desirable, then results may be qualified. Sample results associated with quality control data that exceed acceptance criteria will be qualified with an appropriate comment.

- \mathbf{D} = Data reported from a dilution and or multiple dilutions.
- I = Estimated Value, The reported value is between the Laboratory Method Detection Limit (MDL) and the Laboratory Practical Quantitation Limit (PQL)
- J = Estimated Value
- L = Off-Scale high; exceeds the linear range or highest calibration standard.
- O = Sampled, but analysis lost or not performed
- Q = Sample held beyond normal holding time
- U = indicates the compound was analyzed for, but not detected. The numerical value preceding the "U" is the limit of detection for that compound based upon the dilution. MEDF = Matrix Effected Dilution Factor.
- V = Analyte was detected in both the sample and associated Laboratory Method Blank; Laboratory Contamination
- \mathbf{Y} = The analysis was from an unpreserved or improperly preserved sample. The data may not be accurate

Unless otherwise noted, ug/Kg and mg/Kg denote dry weight.

(SOILS) Actual Reporting Limit will depend on moisture content of sample and the amount of sample received.

LCS Obs. Value is the observed quantity, as calculated from the calibration curve, of the analyte in the Laboratory Control Sample (LCS). The LCS is a standard from a source different than the source of the standards used for calibration. The LCS is also known as the QC sample. It is used to check the accuracy of the calibration curve.

Form FD 9000-24 GROUNDWATER SAMPLING LOG

												Rise	r: 2.8
SITE NAME:	Allison c	2955	PS#F	3215	SI L(TE DCATION:	2	orlan	Lo, FC	-			
SITE NAME:Allison OgksPS#F3215SITE LOCATION:Orlando, FC.WELL NO:PS#F3215SAMPLE ID:PS#F3215DATE:9/20/12													
						GING DA							
WELL DIAMETEI	R (inches):	r TUBIN DIAM	IG ETER (inches):	1/811 WE	LL SCREEN PTH: 3_0 fe	INTERVAL set to /3,0 f	feet	STATIC E	EPTH ER (feet): 8.7 WELL CAPAC	9		E PUMP T	YPE Ar
	t if applicable)									ITY			
EOUIDME				<u>15,0</u>	feet - Ž	7.74 RING CARACI		feet) X	JBING LENGTH		s/foot	= C,	ZS gallons
	t if applicable)	URGE: TEG								,	VUELL		
		IG	FINAL PUI		allon <u>s + (</u>	PURGIN		oot X	PURGING) +	-	gallons TOTAL VO	-
	WELL (feet):	11,5'		WELL (feet):	14,5			т:0957	ENDED AT:	10/2	; F	PURGED (gallons): 0.97
TIME	VOLUME PURGED (gallons)	CUMUL. VOLUME PURGED (gallons)		DEPTH TO WATER (feet)	pH (standard units)	темр. (°С)	(cìr	COND. rcle units) nho3/cm r S/cm	DISSOLVED OXYGEN (circle units) rhg/L <u>or</u> Saturation		BIDITY Us)	COLC (descrit	
0957	0.25	0.25	,06	13.05	6.44	25,16	5	83	\$0,8% 5.01	7.0	2	Clear	non
6000	0118	0.43	,06	13.84	6.14	25.13			58.8% 4.89			eL	11
1003	6.18	0.61	106	13.85	5.89	25.07			60,T/./5.0	5,5		eL	11
1006	0.12	0.73	,04	14.23	5.71	25.05			59,8/0/4,92			66	47
1009	0,12	0,85	,04	14.35	5.62	25,05			<u>59.5// 4.96</u>			CC	(/
1012	0.12	0.97	104	14,48	5.57	25/06	20	62	60% 4.95	2.4	(CL	11
				-									
				_									
WELL CA	PACITY (Gallor	s Per Foot):	0.75" = 0.02; /Ft): 1/8" = 0	1" = 0.04; 0006: 3/16'	1.25'' = 0.0	6; 2" = 0.10 1/4" = 0.002	6; 6;		4 " = 0.65; 004; 3/8 " = 0	5'' = 1.02		" = 1.47; 0.010;	12" = 5.88 5/8" = 0.016
	EQUIPMENT (BP = Bladder F		SP = Electric			mp; PP = P	eristaltic	_		ther (Specify)
						LING DA	AT	4					
	BY (PRINT) / A			SAMPLER(S)					SAMPLING INITIATED A	т. / с. /	.	SAMPLIN	IG AT: ;;;;;;;]
PUMP OR	BURAS /		sa	TURING	1 pour			FIELD	FILTERED: Y		1		ize: m
DEPTH IN	WELL (feet):	14.5		MATERIAL C				Filtratio	on Equipment Ty	/pe:			
	CONTAMINATI			D	TUBING	Y Ø(re		ed)	DUPLICATE				
SAM SAMPLE	PLE CONTAINE	ER SPECIFIC		PRESERVAT		RESERVATIO	N	FINAL	INTEND ANALYSIS A			MPLING NPMENT	SAMPLE PUMP FLOW RATE
ID CODE	CONTAINERS	CODE	VOLUME	USED		D IN FIELD (r	mL)_	pH	МЕТНО	D	C	ODE	(mL per minute)
F3215	2	CG	YOML	Hec		~			VOA_		RF	-pp	Cloome
	2	AG	YOML	Lone					Toc_				LIGORL
	2	CG	YORL	Hec		-		~	LL Merc			4	<100 MC
	<u> </u>	AG	ILFr.	How		<u> </u>	_	~	FCIPRO		-101	~	1046pin
	1	AG	1640.	Non		<u> </u>			8270-5In				
REMARKS	· · · · ·	PE PE	250mL 125mL	HN03		-		 	Hex Cr 4 meta	15	-		₽ ∕
	p down	due to	droping	xater In	wellA	llow re	chy	irse fu	5 Smin		to	Collec	fing Samples
MATERIA		AG = Ambe		Clear Glass;	PE = Poly			Polypropyl	ene; S = Silic	one; T	= Teflo	n; 0 = (Diher (Specify)
SAMPLING	G EQUIPMENT		APP = After Pe RFPP = Revers		B = Bai Itic Pumo:			der Pump; od (Tubing	ESP = Elect Gravity Drain):				
RFPP = Reverse Flow Peristallic Pump; SM = Straw Method (Tubing Gravity Drain); O = Other (Specify)													

NOTES: 1. The above do not constitute all of the information required by Chapter 62-160, F.A.C.

2. STABILIZATION CRITERIA FOR RANGE OF VARIATION OF LAST THREE CONSECUTIVE READINGS (SEE FS 2212, SECTION 3)

pH: \pm 0.2 units Temperature: \pm 0.2 °C Specific Conductance: \pm 5% Dissolved Oxygen: all readings \leq 20% saturation (see Table FS 2200-2); optionally, \pm 0.2 mg/L or \pm 10% (whichever is greater) Turbidity: all readings \leq 20 NTU; optionally \pm 5 NTU or \pm 10% (whichever is greater)

DEP-SOP-001/01 FT 1000 General Field Testing and Measurement

				D INSTRUME					
INSTRUM	ENT (M	AKE/MOD	EL#) _	<u>YSI 556MP</u>	S	INSTRUM	ENT # _06H	251 <u>0AF</u>	
PARAME	TER: [c	heck only o	one]						
🗌 TEM	🗌 TEMPERATURE 🛛 🖾 CONDUCTIVITY 🗌 SALINITY 🕅 pH 🗌 ORP								
🗌 TUR	BIDITY		RESIDUAL	_ CI 🔀 D	0	🗌 ОТН	ER		
	STANDARDS: [Specify the type(s) of standards used for calibration, the origin of the standards, the standard values, and the date the standards were prepared or purchased]								
Standa	ard A	Do 1	000 /0						
Standa	ard B	PH	4,7,	0					
Standa	ard C	Conducti	uity	1413					
DATE (yy/mm/dd)	TIME (hr:min)	STD (A, B, C)	STD VALUE	INSTRUMENT RESPONSE	% DEV	CALIBRATED (YES, NO)	TYPE (INIT, CONT)	SAMPLER INITIALS	
9/20/12	0925	A	100%	92.0 /100,3	8%/c1	Yes	Init	mb	
1	0934	B	4.0	4.03	21		1		
	0443	ß	2.0	6.97	21	}			
	0949	ß	10.0	10.10	10/0				
	0951	С	1413	1400	<1	1	1	4	
9/20/12	1157	A	100%	1.00.4%	<1	Yes	cont	MB	
	1200	ß	4	4.01	41			1	
	1203	ß	7	7,0	<1			>	
	1208	ß	10	10.03	<i><</i> [
	1211	e	1413	1413	41	d'	, r		
				-					
	1					,			
	1								
	I		I		l			ļ	

`

*

DEP-SOP-001/01 FT 1000 General Field Testing and Measurement

	Form	ו FD 9000	-8: FIEL	D INSTRUME	NT CALI	BRATION R	ECORDS	
INSTRUM	ENT (M	AKE/MOD	EL#) <u>I</u>	HACH 2100P		RUMENT #	08080C017	245
PARAME	TER: [c/	heck only d	one]					
🗌 TEM	PERATUR	RE 🗍 (CONDUCT		SALINITY	🗌 рН	ORP	
🗹 TUR	BIDITY		RESIDUAL	. CI 🗌 [00	🗌 ОТН	ER	
				ndards used for c ared or purchase		he origin of the	standards, the	standard
Standa	ard A	<0.1					_	
Standa	ard B	20.0						
Standa	ard C	100						
DATE (yy/mm/dd)	TIME (hr:min)_	STD (A, B, C)	STD VALUE	INSTRUMENT RESPONSE	% DEV	CALIBRATED (YES, NO)	TYPE (INIT, CONT)	SAMPLER INITIALS
9/20/12	0921	A	0.(0,14 0.11	60/10/	(es	Zait	MB.
	0923	ß	20.0	20,2	1%			1
J	0925	Ċ	100	99.3	21			
glolic	1213	A	0.)	0,11	1%	405	cowf	1417
	1214	ß	20,0	2011	21		1	
	1215	Ś	1,00	99.7	01			
	/		V					
					_			
			ļ		_			
							-	

DATE: 9/19/19 SITE: Pump Station #3215 LOCATION: O, lando, FL. WELL LOCATION STRATEGY: 7 MW-3 DRILLING COMPANY: Groundwater Protection DRILLING METHOD / BORING DIAMETER: Geo Probe / 4" WELL DEPTH / SCREEN INTERVAL: 13 bls / 3 - 13' GROUNDWATER LEVEL: 9.87' TOC TOP OF CASING ELEVATION: DEVELOPMENT PROCEDURE: Peristaltic Pump DISPOSITION OF INVESTIGATIVE DERIVED WASTES: Spread **REMARKS:** PROTECTIVE CASING TYPE: <u>NA</u> LOCKING CAP: Y/N 2.0'-SURFACE COVER: 91935 Å CEMENT GROUT , a , , , , RISER /" PVC 3,0' -SEAL ____A 13.0' -134.30/65 SCREEN 11,006 Slot Screen 10,0' -FILTER _ 30/63 WELL POINT

Terracon



NODARSE



Geotechnical Engineering Report

Greenview Pines Pump Station No. 3887

Orlando, Florida October 16, 2012 Project No. AK125005

Prepared for:

Orange County Public Utilities-Engineering Division Orlando, Florida

Prepared by:

Nodarse & Associates A Terracon Company Winter Park, Florida





October 16, 2012

Orange County Public Utilities – Engineering Division 9150 Curry Ford Road Orlando, Florida 32815

Attn: Mr. Jeff Nazario

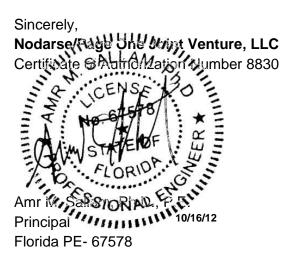
Re: Geotechnical Engineering Report Greenview Pines Pump Station No. 3887 Orlando, Florida Project Number: AK125005

Dear Mr. Nazario:

Nodarse/Page One Joint Venture has completed the geotechnical engineering services for the above referenced project. This study was performed in general accordance with our proposal number PH1120208 dated May 2, 2012.

This report presents the findings of the subsurface exploration and provides geotechnical recommendations concerning earthwork and the design and construction of the proposed wet well pump station.

We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report, or if we may be of further service, please contact us.



Enclosures cc: 1 – Client (PDF) 1 – File Jay W. Casper, P.E. Senior Associate Florida PE - 36330

EXECL	JTIVE S	SUMMARY	i
1.0	INTRO	DUCTION	1
	2.1	Project Description	1
	2.2	Site Location and Description	2
3.0	SUBSL	JRFACE CONDITIONS	2
	3.1	USDA Soil Survey	2
	3.2	Typical Profile	2
		Groundwater	
4.0	RECO	MMENDATIONS FOR DESIGN AND CONSTRUCTION	4
	4.1	Geotechnical Considerations	4
		4.1.1 Pump Station:	4
		4.1.2 Pipelines:	5
		4.1.4 General Site Preparation	
		4.1.5 Temporary Dewatering:	
5.0	GENE	RAL COMMENTS	7

APPENDIX A – FIELD EXPLORATION

Exhibit A-1	Site Location Map
Exhibit A-2	Soil Survey Map
Exhibit A-3	Soil Survey Descriptions
Exhibit A-4	Boring Location Plan
Exhibit A-5	Field Exploration Description
Exhibit A-6 to A-9	Boring Logs

APPENDIX B – SUPPORTING INFORMATION

APPENDIX C – SUPPORTING DOCUMENTS

Exhibit C-1	General Notes
Exhibit C-2	Unified Soil Classification System

APPENDIX D – SUSTAINABILITY CONSIDERATIONS

Exhibits D-1 to D-3 Sustainability Considerations



EXECUTIVE SUMMARY

A geotechnical investigation has been performed for the proposed Greenview Pines Pump Station planned at 3955 Greenview Pines Court in Orlando, Orange County, Florida. Three (3) borings, designated AB-01, AB-02, and TB-01 have been performed to depths of between 10 and 50 feet below the existing ground surface within the pump station areas. This report specifically addresses the recommendations for the proposed pump station wet well, manhole, and pipelines.

Based on the information obtained from our geotechnical exploration, it appears that the subsoil and groundwater conditions at the site are suitable for the proposed developed and construction. The following geotechnical considerations were identified:

- Temporary dewatering will be required for construction of the pump station. Dewatering the pump station area will require the use of a properly designed well point system. The dewatering system should not be turned off until the pump station has enough dead weight to counteract an uplift force calculated based on a head of water measured from the base of the pump station to the estimated Seasonal High Water Level (SHWL).
- Our borings did not encounter unsuitable soils such as muck, clay, high silts, and debris, which might cause problems during construction. However, if encountered, unsuitable soils should be completely removed to a minimum depth of 18 inches below the pump station pipelines bottom, replaced with well-draining granular sands with a fines content of 5 percent or less passing the No. 200 U.S. Standard sieve by weight, and compacted to a firm and unyielding state.
- The proposed structure may be supported on shallow footings bearing on the existing site soil only if the proper site preparations are following according to the appropriate sections of this report.
- On-site native soils typically appear suitable for use as general engineered fill.

This summary should be used in conjunction with the entire report for design purposes. It should be recognized that details were not included or fully developed in this section, and the report must be read in its entirety for a comprehensive understanding of the items contained herein. The section titled **GENERAL COMMENTS** should be read for an understanding of the report limitations.

GEOTECHNICAL ENGINEERING REPORT GREENVIEW PINES PUMP STATION NO. 3887 ORLANDO, FLORIDA Project No. AK125005 October 16, 2012

1.0 INTRODUCTION

A geotechnical engineering report has been prepared for the proposed Greenview Pines Pump Station which will be located at 3955 Greenview Pines Court in Orlando, Orange County, Florida as shown on the Topographic Vicinity Map included as Exhibit A-1 in Appendix A. Three (3) borings, designated AB-01, AB-02, and TB-01 have been performed to depths of between 10 and 50 feet below the existing ground surface in the proposed pump station and manhole area. Logs of the borings along with a site location plan, geologic map and boring location plans are included in Appendix A of this report.

The purpose of the geotechnical services was to provide information and geotechnical engineering recommendations relative to the proposed pump station wet well, gravity pipeline, and a concrete drive way. The followings will be provided:

- Field exploration method
- Subsurface soil and groundwater conditions
- Presentation of field and laboratory information in graphical format
- Recommendations for general earthwork
- Recommendations for pump station design and construction
- Recommendations for gravity pipe line earthwork

2.0 **PROJECT INFORMATION**

2.1 **Project Description**

Item	Description					
Site layout	See Appendix A, Exhibit A-4: Boring Location Plan					
Construction	One wet well to a depth of about 20 feet below existing grade and 6 feet in diameter with associated pipelines and man holes.					
Grading	Fill – fine grading, estimated at up to approximately 1 foot.					
Cut and fill slopes	Excavation per OSHA requirements or a license professional engineer for braced excavations.					



2.2 Site Location and Description

Item	Description
Location	The project will be located at 3955 Greenview Pines Court in Orlando, Orange County, Florida
Existing improvements	No existing structures on site. A residential structure exists just south of the site.
Current ground cover	Grass covered with limited trees.
Existing topography	The USGS topographic quadrangle map "Orlando East, Florida" and "Oviedo SW, Florida" depict the developed topography as nearly level, with original ground surface elevations ranging from about elevation +60 feet to +65 feet referencing the National Geodetic Vertical Datum of 1929 (NGVD29).

3.0 SUBSURFACE CONDITIONS

3.1 USDA Soil Survey

The Soil Survey of Orange County, Florida, as prepared by the United States Department of Agriculture (USDA), Soil Conservation Service (SCS; later renamed the Natural Resource Conservation Service - NRCS), dated October 1981, identifies the soil types at the project site as Pomello fine sand, 0 to 5 percent slopes (34). It should be noted that the Soil Survey is not intended as a substitute for site-specific geotechnical exploration; rather it is a useful tool in planning a project scope in that it provides information on soil types likely to be encountered. A copy of the pertinent section of the Soil Survey map is included as Exhibit A-2 in Appendix A. Descriptions of soil map units are included in Appendix A as Exhibit A-3.

3.2 Typical Profile

Based on the results of the borings, subsurface conditions on the project site can be generalized as follows:

Stratum	Approximate Depth to Bottom of Stratum (feet)	Consistency/ Density		
1	8	Fine sand to fine sand with silt (SP/SP-SM)	Loose to medium dense	
2	10 to 13.5	Silty fine sand (SM)	Loose	



Stratum	Approximate Depth to Bottom of Stratum (feet)	Material Description	Consistency/ Density		
3	15 to 50	Fine sand to fine sand with silt (SP/SP-SM)	Loose to dense		

Conditions encountered at each boring location are indicated on the individual boring logs. Stratification boundaries on the boring logs represent the approximate location of changes in soil types; in-situ, the transition between materials may be gradual. Details for each of the borings can be found on the boring logs in Appendix A of this report. Descriptions of our field exploration are included as Exhibit A-5 in Appendix A. Descriptions of our laboratory testing procedures are included as Exhibit B-1 in Appendix B.

3.3 Groundwater

The boreholes were observed during drilling for the presence and level of groundwater. Groundwater was observed in the borings at a depth of 4.5 feet below existing grade. It should be recognized that fluctuations of the groundwater table will occur due to seasonal variations in the amount of rainfall, runoff and other factors not evident at the time the boring was performed. Therefore, groundwater levels during construction or at other times in the future may be higher or lower than the levels indicated on the boring logs. The estimated seasonal high groundwater tables are included in the following table and on the boring logs.

Boring #	Approximate depth to encountered water table (feet)	Approximate depth to estimated normal seasonal high groundwater table (feet)
AB-01	4.5	3
AB-02	4.5	3
TB-01	4.5	3

Estimates of the normal seasonal high water table presented in this report are based on and limited by the data collected during our geotechnical exploration, and the referenced published documents. Estimates of the normal seasonal high assume normal precipitation volumes and distribution. These seasonal water table estimates do not represent the temporary rise in water table that occurs immediately following a storm event, including adjacent to other stormwater management facilities. This is different from static groundwater levels in wet ponds and/or drainage canals which can affect the design water levels of new, nearby ponds. The seasonal high water table may be affected by extreme weather changes, localized or regional flooding, karst activity, future grading, drainage improvements, or other construction that may occur on our around the site following the date of this report.



4.0 **RECOMMENDATIONS FOR DESIGN AND CONSTRUCTION**

4.1 Geotechnical Considerations

The following conclusions and recommendations are based on the project characteristics previously described, the data obtained in our field exploration and our experience with similar subsurface conditions and construction types. If the proposed pump station location is significantly different from that previously described, or if subsurface conditions different from those disclosed by the borings are encountered during construction, we should be notified immediately so that we might review and modify, if necessary, the following recommendations in regards to such changes. The general guidelines included in this report are not intended to supersede more stringent requirements which may be mandated by County specifications.

4.1.1 Pump Station: Boring TB-01 was performed near the approximate location of the proposed pump station wet well as indicated by provided site plans. Groundwater was encountered in the boring at a depth of about 4.5 feet below existing grade. Based on the provided plans, the anticipated depth of the proposed pump station wet well is to be about 20 feet below existing grade.

- Dewatering will be required for construction of the pump station. Dewatering the pump station area will require the use of a properly designed well point system. Other dewatering systems utilizing sumps within shored or braced excavations may also be feasible. However, design of shoring/sump systems should be carefully evaluated with regard to blow outs of the excavation bottom due to unbalanced hydrostatic conditions. The Contractor should be allowed to review the soil stratification to determine the most feasible dewatering system for the pump station area. Dewatering should be performed gradually and slowly in order to reduce the effect of the sudden additional effective stress increase on the subsoil below close-by housed or roadways.
- All excavation should be performed in accordance with appropriate Occupational Safety and Health Administration (OSHA) standards. These standards typically include side slopes for temporary excavation no steeper than 1.5 horizontal to 1 vertical (1.5H: 1V) to provide adequate worker safety.
- If these side slopes cannot be maintained or are not desired due to other considerations, a properly designed and braced excavation or sheet piling would be required. All shoring and bracing systems or sheet piling should be designed and reviewed by an experienced professional engineer registered in the State of Florida.



Although not encountered, it is important to note that soils with high fines content (clay, silts, ect.) or unsuitable material (organics, muck, debris, ect.) should be removed to a minimum depth of 12 inches below the pump station bottom, to provide a stable construction platform, and replaced with well-draining granular sands with fines contents of 5 percent of less passing the No. 200 U.S. Standard sieve by weight. The soils below the base of the pump station should be compacted to a firm and unyielding state.

After the subgrade soils have been prepared as recommended above, the pump station may be supported on a monolithic slab or spread footing. The foundations can utilize a maximum net soil bearing pressure of 2,000 pounds per square foot.

- Compaction of backfilled soils around the pump station should be accomplished in lift thicknesses no greater than 8 inches. The fill material should consist of relatively clean granular sands with no more than 5 percent passing the No. 200 U.S. standard sieve by weight.
- Compaction can likely be accomplished in these areas with a small plate or hand guided drum type vibratory compactor and loose lift thicknesses should be limited to 8 inches. At least one (1) density test should be performed on each lift to verify that the soil has been compacted to at least 95 percent of its modified Proctor maximum dry density (ASTM D-1557).
- If compaction difficulties arise during construction, the geotechnical engineer should be consulted to provide further recommendations.
- The construction should also be sequenced so that a dewatering system, if necessary, is not turned off until the pump station has enough weight to counteract an uplift force equivalent to the amount of water displaced. It may also be prudent to place additional concrete in the structure foundation to provide ballast against such an uplift force. This uplift force should account for the head difference from the bottom elevation of the foundation to the seasonal high groundwater level or the groundwater level at the time of construction, whichever is shallower, plus any possible flooding conditions that may occur at the project site.
- For calculations of resistance to the uplift force, 50 pounds per cubic foot may be used for the buoyant unit weight of the soil. The buoyant weight of the concrete and overlying soils should be used in calculating the necessary amount of ballast required.

4.1.2 Pipelines: Regarding the pipe subgrade soils and backfill soils we offer the following recommendations:



- The bedding soil beneath the pipe should be properly shaped to completely support the pipe section and areas should be excavated to accommodate any bells or other raised portions of the pipe to help avoid point loading conditions.
- Once the pipe has been laid in the excavation trench and approved, backfill should be carefully deposited and compacted to the centerline of the pipe on both sides. All fill should be inorganic, non-plastic, granular soils (clean sands). The near surficial native site soils appear to meet backfill requirements.
- Compaction of backfilled soils above the centerline of the pipe to the proposed final grade should be accomplished in lift thicknesses no thicker than 12 inches.
- At least one (1) density per lift should be performed to verify that the soil has been compacted to 95 percent of the material's maximum modified Proctor dry density (ASTM D 1557).
- If compaction difficulties arise during construction, the Geotechnical Engineer should be consulted to provide further recommendations.

4.1.4 General Site Preparation: The following general procedures are recommended for site preparation:

- All excavations required should be performed in accordance with appropriate Occupational Safety and Health Administration (OSHA) standards. These standards typically include side slopes for temporary excavations not steeper than 1.5 Horizontal to 1 Vertical (1.5H:1V) to provide for adequate worker safety.
- If these side slopes cannot be maintained or are not desired due to other considerations, a properly designed braced excavation, trench shield, or sheet piling would be required for stable excavations. All shields, shoring and bracing systems, or sheet piling should be designed and reviewed by an experienced Professional Engineer registered in the State of Florida. Adjacent traffic loads and induced vibrations, among other factors, should be included in the design of these stabilization systems.

4.1.5 Temporary Dewatering: Groundwater was observed at a depth of about 4.5 feet at our boring locations at the time of our exploration. The normal seasonal high groundwater level is anticipated to be at a depth of about 3 feet below existing grades. Based on this information and the proposed embedment depths of the pump station, dewatering will be required to



facilitate construction, backfill and compaction in the dry. Regarding dewatering, we offer the following recommendations:

- Dewatering operations at this site for the proposed pump station should be accomplished with a properly designed well point system dewatering system operating outside the excavation limits.
- The dewatering system should be adequate to lower groundwater levels to at least 2 feet below the lowest compaction surface.
- Other dewatering systems utilizing sumps within shored or braced excavations may also be feasible. However, design of shoring/sump systems should be carefully evaluated with regard to blow outs of the excavation bottom due to unbalanced hydrostatic conditions. The Contractor should be allowed to review the soil stratification to determine the most feasible dewatering system for the pump station area.

The construction should be sequenced so that the dewatering system is not turned off until the pump station has enough weight placed over it to counteract an uplift force equivalent to the height of standing water above the base of the pump station. The resisting weight of soil over the pump station should be calculated using the buoyant unit weight of the soil.

5.0 GENERAL COMMENTS

Terracon should be retained to review the final design plans and specifications so comments can be made regarding interpretation and implementation of our geotechnical recommendations in the design and specifications. Terracon also should be retained to provide observation and testing services during grading, excavation, foundation construction and other earth-related construction phases of the project.

The analysis and recommendations presented in this report are based upon the data obtained from the borings performed at the indicated locations and from other information discussed in this report. This report does not reflect variations that may occur between borings, across the site, or due to the modifying effects of construction or weather. The nature and extent of such variations may not become evident until during or after construction. If variations appear, we should be immediately notified so that further evaluation and supplemental recommendations can be provided.

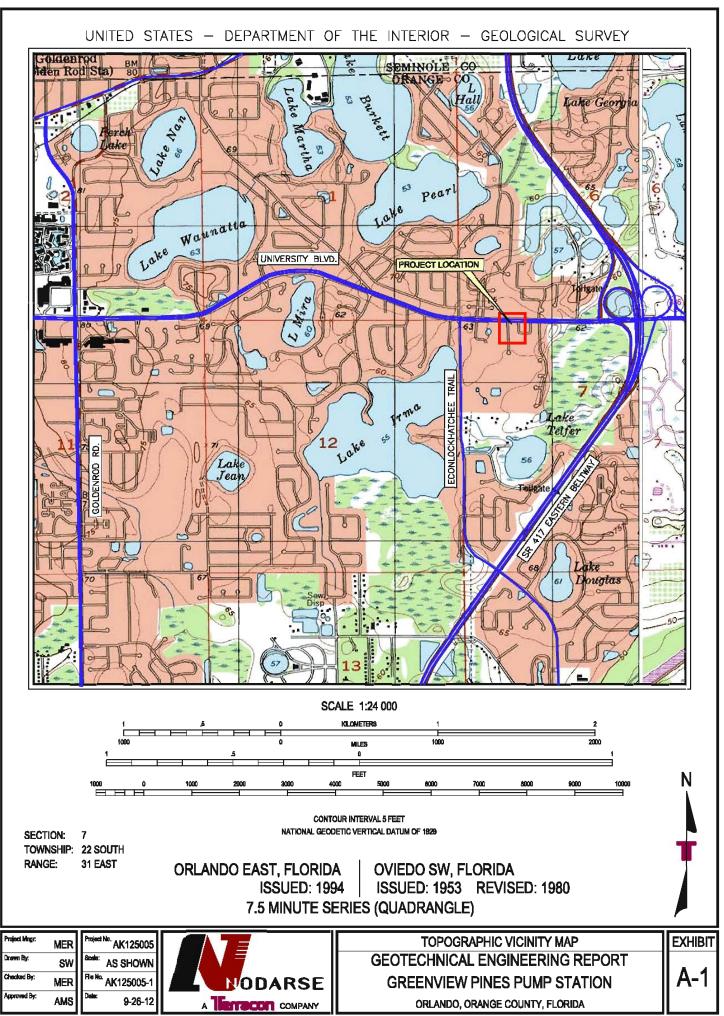
The scope of services for this project does not include either specifically or by implication any environmental or biological (e.g., mold, fungi, bacteria) assessment of the site or identification or

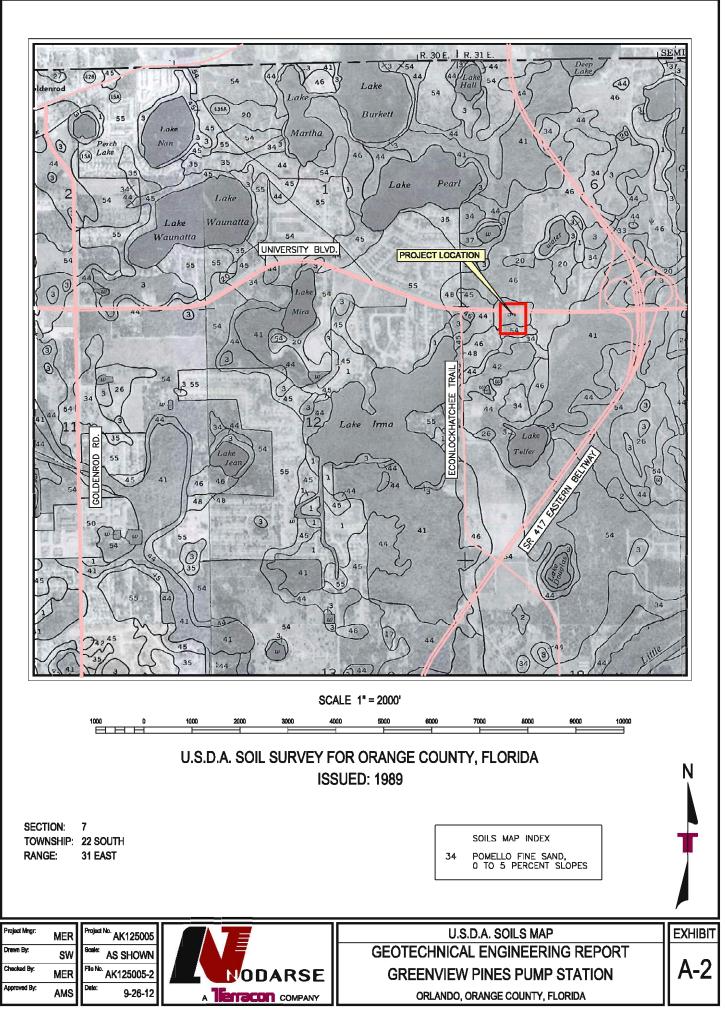


prevention of pollutants, hazardous materials or conditions. If the owner is concerned about the potential for such contamination or pollution, other studies should be undertaken.

This report has been prepared for the exclusive use of our client for specific application to the project discussed and has been prepared in accordance with generally accepted geotechnical engineering practices. No warranties, either express or implied, are intended or made. Site safety, excavation support, and dewatering requirements are the responsibility of others. In the event that changes in the nature, design, or location of the project as outlined in this report are planned, the conclusions and recommendations contained in this report shall not be considered valid unless Terracon reviews the changes and either verifies or modifies the conclusions of this report in writing.

APPENDIX A FIELD EXPLORATION

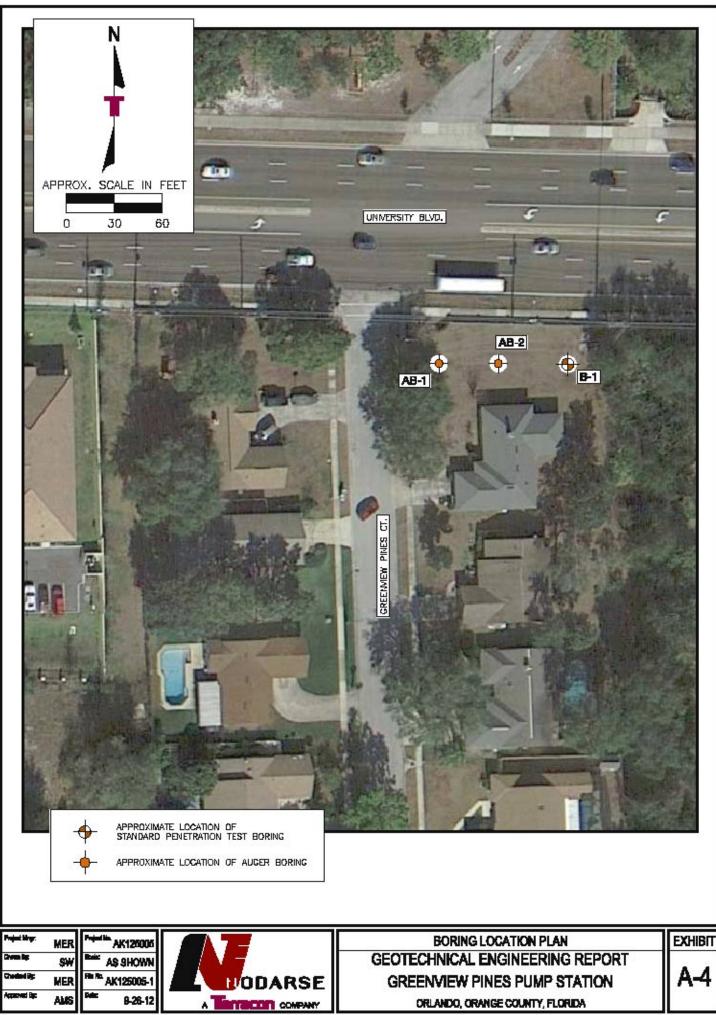






Soil Survey Descriptions

<u>34 – Pomello fine sand, 0 to 5 percent slopes.</u> This soil type is nearly level to gently sloping and moderately well drained. It is typically found on low ridges and knolls on the flatwoods. In its natural state and during years of normal rainfall, this soil type has a seasonal high water table at a depth of between 20 and 40 inches (1.7 and 3.3 feet) for 1 to 4 months, receding to a depth of 40 to 60 inches (3.3 to 5.0 feet) during dry periods.





Field Exploration Description

The boring locations were laid out at the project site by Terracon personnel. The locations indicated on the attached diagram are approximate and were measured by pacing distances and estimating right angles. The locations of the borings should be considered accurate only to the degree implied by the means and methods used to define them.

The SPT soil borings were drilled with a mini-rig mounted, rotary drilling rig equipped with a rope an automatic hammer. The boreholes were advanced with a cutting head and stabilized with the use of bentonite (drillers' mud). Soil samples were obtained by the split spoon sampling procedure in general accordance with the Standard Penetration Test (SPT) procedure. In the split spoon sampling procedure, the number of blows required to advance the sampling spoon the last 12 inches of an 18-inch penetration or the middle 12 inches of a 24-inch penetration by means of a 140-pound hammer with a free fall of 30 inches, is the standard penetration resistance value (N). This value is used to estimate the in-situ relative density of cohesionless soils and the consistency of cohesive soils. The sampling depths and penetration distance, plus the standard penetration resistance values, are shown on the boring logs.

Portions of the samples from the borings were sealed in glass jars to reduce moisture loss, and then the jars were taken to our laboratory for further observation and classification. Upon completion, the boreholes were backfilled with the site soil.

Field logs of each boring were prepared by the drill crew. These logs included visual classifications of the materials encountered during drilling as well as the driller's interpretation of the subsurface conditions between samples. The boring logs included with this report represent an interpretation of the field logs and include modifications based on laboratory observation of the samples.

	BORING LOG NO. AB-01								Page 1 of 1					
	PROJECT: Greenview Pines Pump Station No. 3887 SITE: 3955 Greenview Pines Court Orlando, Florida				CLIENT: O.C. Public Utilities - Engineering Division Orlando, Florida									
	GRAPHIC LOG		N See Exhibit A-3				DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	Percent Fines		
		DEPTH FINE	SAND (SP), brown to gray				_							
SMART LOG-DEPTH TO BOTTOM OF PAGE AK125005 BORING LOGS GPJ ODOT TEST GPJ 10/16/12		6.5												
DT TEST.(SAND (SP), light brown				_							
S.GPJ ODC			<mark>Y FINE SAND (SM)</mark> , brown				-	-			31	23		
NG LOG			ng Terminated at 10 Feet				10							
005 BORI							_							
E AK1250							-							
OF PAGE							15-							
OTTOM							_							
тн то в							_							
OG-DEP							_	-						
MART L							20-							
							_							
IAL REP							-	-						
I ORIGIN							- 25-							
ED FROM														
PARATE		Stratificatio	on lines are approximate. In-situ, the transition m	ay be gradual.										
THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT.	Advancement Method: Continuous Auger		See Exhibit A-4 for desc procedures See Appendix B for des procedures and addition	escription of laboratory onal data, (if any).										
G IS NO	Abandonment Method: See A Borings backfilled with cement-bentonite grout upon completion. WATER LEVEL OBSERVATIONS			See Appendix C for exp abbreviations.	lanation of symbols and									
ING LO						Boring Starte	d: 9/17	/2012		Boring Completed	: 9/17/20	012		
S BOR	GWT Encountered During Drilling			۲.		Drill Rig: Mini Rig Driller: Mark C.								
THIS	ව 1675 Lee I E Winter Park,				Project No.: A	No.: AK125005 Exhibit A-6								

BORING LOG NO. AB-02 Page 1 of 1									
PROJECT: Greenview Pines Pump Station No. 3887 CLIENT: O.C. Public Ut Orlando, Florid					ngin				
SITE: 3955 Greenview Pines Court Orlando, Florida									
DEPTH			DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	Percent Fines	
FINE SAND (SP), brown					T				
1.5 SILTY FINE SAND (SM), grayish-brown							11	18	
6.5 FINE SAND WITH SILT (SP-SM), grayish-br	own		-						
Boring Terminated at 10 Feet			10-						
			_ _ 15—						
			20						
Chatification lines are convoluente la situ des transitions			25— _						
Stratification lines are approximate. In-situ, the transition r	nay be gradual.								
Advancement Method: Continuous Auger Abandonment Method: Borings backfilled with cement-bentonite grout upon completion.	See Exhibit A-4 for description procedures See Appendix B for description procedures and additional data See Appendix C for explanatic abbreviations.	n of laboratory ı, (if any).							
				ted: 9/17/2012 Boring Completed: 9/17/2012					
GWT Encountered During Drilling Drill Rig: Mini				ni Rig Driller: Mark C.					
	Winter Park, Florida Project No.: A					Exhibit A-7			

	BORING LOG NO. TB-01 Page 1 of 2									2		
	PR	OJECT:	Greenview Pines Pump Station No. 3887			O.C. Public L Orlando, Flor		s - E	ngin			
	SIT	ſE:	3955 Greenview Pines Court Orlando, Florida									
	GRAPHIC LOG	LOCATION	N See Exhibit A-3				DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	Percent Fines
			SAND (SP) , brown to grayish-brown, lo	ose to medium dens	e		-			3-3-3-3 N=6		
							-		M	3-4-5-6 N=9		
PJ 10/16/12							5-		X	5-4-7-6 N=11		
DOT TEST.GI		8.0						X	7-7-6-5 N=13			
OGS.GPJ OI		SILT	<u>/ FINE SAND (SM)</u> , light grayish-brown	, 100Se			- 10-		X	5-4-5-5 N=9	16	16
H TO BOTTOM OF PAGE AK125005 BORING LOGS.GPJ ODOT TEST.GPJ 10/16/12							-	-				
DF PAGE AK1		13.5 FINE	SAND WITH SILT (SP-SM), light brown	, medium dense					X	6-6-8 N=14		
FO BOTTOM (-	-				
SMART LOG-DEPTH '							-			6-7-7 N=14		
							20-					
GINAL REPOF							-			10-10-11		
FROM ORI							25-	-	\square	N=21		
PARATED		Stratificatio	on lines are approximate. In-situ, the transition m	ay be gradual.		Hammer	Type: R	ope ar	d Cath	nead		
THIS BORING LOG IS NOT VALID IF SEPARATED FROM ORIGINAL REPORT.	Rot	cement Meth ary Drilling C	utting Head	See Exhibit A-4 for deso procedures See Appendix B for des procedures and addition See Appendix C for exp	cription of laboranal data, (if any)							
N SI DC	Bor	ings backfille pletion.	d with cement-bentonite grout upon	abbreviations.						-		
SING LC	∇		R LEVEL OBSERVATIONS		ODARSE	Boring Star	Started: 9/17/2012 Boring Completed: 9/17/20					
S BOF				۲.	ee Road	Drill Rig: M	Drill Rig: Mini Rig Driller: Mark C.					
THI	Winter Park, Florida				Project No.	Project No.: AK125005 Exhibit A-8						

		B	ORING LO	G NO.	TB-0	01				Pag	e 2 of 2	2
PR	OJECT:	Greenview Pines Pump Station No. 3887		CLIENT:	O.C. F Orland	Public Ut do, Flori	ilities da	6 - E	ngin	eering Divis		
SIT	'E:	3955 Greenview Pines Court Orlando, Florida										
GRAPHIC LOG	LOCATIO	N See Exhibit A-3					DEPTH (Ft.)	WATER LEVEL OBSERVATIONS	SAMPLE TYPE	FIELD TEST RESULTS	WATER CONTENT (%)	Percent Fines
		SAND WITH SILT (SP-SM), light brown	, medium dense <i>(cor</i>	ntinued)			_	-				
		SAND (SP) , light gray to light brown, m	edium dense to dens	se			 30 -	-	X	12-16-14 N=30		
							- 35 -	-	X	10-10-12 N=22		
	38.5 FINE	<u>SAND WITH SILT (SP-SM)</u> , dark gray to	o dark greenish-gray	, loose to me	edium de	nse	- 40- -	-	X	12-8-11 N=19		
							- 45 - -	-	X	4-5-4 N=9		
	50.0						- 50-		X	5-5-5 N=10		
	Borii	ng Terminated at 50 Feet					_	-				
	Stratificatio	on lines are approximate. In-situ, the transition mathematical sectors are approximate.	ay be gradual.			Hammer T	ype: R	ope an	d Cath	lead		
Rota Aband Bori	cement Meth ary Drilling C onment Meth ngs backfille pletion.	utting Head	See Exhibit A-4 for desc procedures See Appendix B for des procedures and addition See Appendix C for exp abbreviations.	cription of labor nal data, (if any)).	Notes:						
$\overline{}$						Boring Starte	ed: 9/17/	/2012		Boring Complete	d: 9/17/20	012
	GWT En	countered During Drilling				Drill Rig: Min	ni Rig			Driller: Mark C.		
				ee Road ırk, Florida		Project No.: /	AK1250	05		Exhibit A-9		

APPENDIX B – LABORATORY TESTING



Laboratory Testing

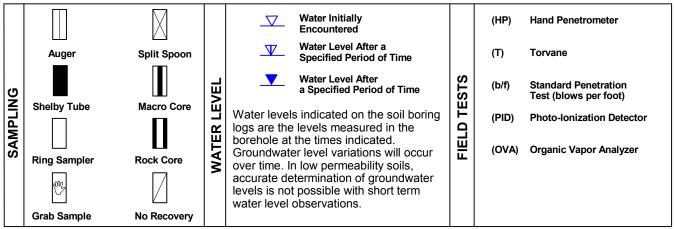
During the field exploration, a portion of each recovered sample was sealed in a glass jar and transported to our laboratory for further visual observation and laboratory testing. Selected samples retrieved from the borings were tested for moisture (water) content and fines content (soil passing a US standard #200 sieve). Those results are included in this report and on the respective boring logs, except for permeability. The visual-manual classifications were modified as appropriate based upon the laboratory testing results.

The soil samples were classified in general accordance with the appended General Notes and the Unified Soil Classification System based on the material's texture and plasticity. The estimated group symbol for the Unified Soil Classification System is shown on the boring logs and a brief description of the Unified Soil Classification System is included in Appendix B. The results of our laboratory testing are presented in the Laboratory Test Results section of this report and on the corresponding borings logs.

APPENDIX C SUPPORTING DOCUMENTS

GENERAL NOTES

DESCRIPTION OF SYMBOLS AND ABBREVIATIONS



DESCRIPTIVE SOIL CLASSIFICATION

Soil classification is based on the Unified Soil Classification System. Coarse Grained Soils have more than 50% of their dry weight retained on a #200 sieve; their principal descriptors are: boulders, cobbles, gravel or sand. Fine Grained Soils have less than 50% of their dry weight retained on a #200 sieve; they are principally described as clays if they are plastic, and silts if they are slightly plastic or non-plastic. Major constituents may be added as modifiers and minor constituents may be added according to the relative proportions based on grain size. In addition to gradation, coarse-grained soils are defined on the basis of their in-place relative density and fine-grained soils on the basis of their consistency.

LOCATION AND ELEVATION NOTES

Unless otherwise noted, Latitude and Longitude are approximately determined using a hand-held GPS device. The accuracy of such devices is variable. Surface elevation data annotated with +/- indicates that no actual topographical survey was conducted to confirm the surface elevation. Instead, the surface elevation was approximately determined from topographic maps of the area.

	(More than Density determin	NSITY OF COARSE-GRAM 50% retained on No. 200 ied by Standard Penetration des gravels, sands and silf	sieve.) on Resistance	CONSISTENCY OF FINE-GRAINED SOILS (50% or more passing the No. 200 sieve.) Consistency determined by laboratory shear strength testing, field visual-manual procedures or standard penetration resistance					
RMS	(Density)	Standard Penetration or N-Value Blows/Ft.	Ring Sampler Blows/Ft.	Descriptive Term (Consistency)	Unconfined Compressive Strength, Qu, psf	Standard Penetration or N-Value Blows/Ft.	Ring Sampler Blows/Ft.		
	Voly Loodo	0 - 3	0 - 6	Very Soft	less than 500	0 - 1	< 3		
RENGTH	Loose	4 - 9	7 - 18	Soft	500 to 1,000	2 - 4	3 - 4		
TREN	Medium Dense	10 - 29	19 - 58	Medium-Stiff	1,000 to 2,000	4 - 8	5 - 9		
S.	Dense	30 - 50	59 - 98	Stiff	2,000 to 4,000	8 - 15	10 - 18		
	Very Dense	> 50	<u>></u> 99	Very Stiff	4,000 to 8,000	15 - 30	19 - 42		
				Hard	> 8,000	> 30	> 42		

RELATIVE PROPORTIONS OF SAND AND GRAVEL

Descriptive Term(s) of other constituents

Trace

With

Modifier

Percent of Dry Weight < 15 15 - 29 > 30

RELATIVE PROPORTIONS OF FINES

Descriptive Term(s) of other constituents Trace With Modifier Percent of Dry Weight < 5 5 - 12 > 12 **GRAIN SIZE TERMINOLOGY**

Major Component of Sample Boulders Cobbles Gravel Sand

Silt or Clay

Over 12 in. (300 mm) 12 in. to 3 in. (300mm to 75mm) 3 in. to #4 sieve (75mm to 4.75 mm) #4 to #200 sieve (4.75mm to 0.075mm Passing #200 sieve (0.075mm)

Particle Size

PLASTICITY DESCRIPTION

<u>Term</u> Non-plastic Low Medium High 0 1 - 10 11 - 30 > 30



UNIFIED SOIL CLASSIFICATION SYSTEM

Criteria for Assigning Group Symbols and Group Names Using Laboratory Tests ^A

Criteria for Assign	ing Group Symbols	and Group Names	S USING Laboratory Tests	Group Symbol	Group Name ^B
	Gravels:	Clean Gravels:	$Cu \geq 4$ and $1 \leq Cc \leq 3^{E}$	GW	Well-graded gravel ^F
	More than 50% of coarse fraction retained	Less than 5% fines ^c	$Cu < 4$ and/or $1 > Cc > 3^{E}$	GP	Poorly graded gravel F
		Gravels with Fines:	Fines classify as ML or MH	GM	Silty gravel F,G,H
Coarse Grained Soils: More than 50% retained	on No. 4 sieve	More than 12% fines ^c	Fines classify as CL or CH	GC	Clayey gravel F,G,H
on No. 200 sieve	Sands:	Clean Sands:	$Cu \ge 6$ and $1 \le Cc \le 3^{E}$	SW	Well-graded sand
	50% or more of coarse fraction passes No. 4 sieve	Less than 5% fines ^D	$Cu < 6$ and/or $1 > Cc > 3^{\text{E}}$	SP	Poorly graded sand ¹
		Sands with Fines:	Fines classify as ML or MH	SM	Silty sand G,H,I
		More than 12% fines ^D	Fines classify as CL or CH	SC	Clayey sand G,H,I
		Inorganic:	PI > 7 and plots on or above "A" line ^J	CL	Lean clay ^{K,L,M}
	Silts and Clays:	morganic.	PI < 4 or plots below "A" line ^J	ML	Silt ^{K,L,M}
	Liquid limit less than 50	Organic:	Liquid limit - oven dried < 0.75	OL	Organic clay K,L,M,N
Fine-Grained Soils: 50% or more passes the		Organic.	Liquid limit - not dried < 0.75	-	Organic silt K,L,M,O
No. 200 sieve		Inorganic:	PI plots on or above "A" line		Fat clay ^{K,L,M}
	Silts and Clays:	morganic.	PI plots below "A" line		Elastic Silt K,L,M
	Liquid limit 50 or more	Organic:	Liquid limit - oven dried < 0.75	ОН	Organic clay K,L,M,P
		Organic.	Liquid limit - not dried		Organic silt K,L,M,Q
Highly organic soils:	Primarily	organic matter, dark in o	PT	Peat	

^A Based on the material passing the 3-inch (75-mm) sieve

^B If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.

^c Gravels with 5 to 12% fines require dual symbols: GW-GM well-graded gravel with silt, GW-GC well-graded gravel with clay, GP-GM poorly graded gravel with clay.

graded gravel with silt, GP-GC poorly graded gravel with clay.
 ^D Sands with 5 to 12% fines require dual symbols: SW-SM well-graded sand with silt, SW-SC well-graded sand with clay, SP-SM poorly graded sand with clay

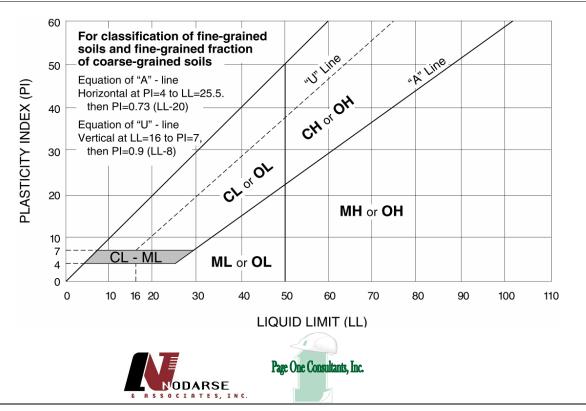
^E Cu = D₆₀/D₁₀ Cc =
$$\frac{(D_{30})^2}{D_{10} \times D_{60}}$$

 $^{\sf F}$ If soil contains \geq 15% sand, add "with sand" to group name. $^{\sf G}$ If fines classify as CL-ML, use dual symbol GC-GM, or SC-SM.

- ^H If fines are organic, add "with organic fines" to group name.
- If soil contains \geq 15% gravel, add "with gravel" to group name.
- ^J If Atterberg limits plot in shaded area, soil is a CL-ML, silty clay.
- ^K If soil contains 15 to 29% plus No. 200, add "with sand" or "with gravel," whichever is predominant.

Soil Classification

- ^L If soil contains ≥ 30% plus No. 200 predominantly sand, add "sandy" to group name.
- ^M If soil contains \geq 30% plus No. 200, predominantly gravel, add "gravelly" to group name.
- ^N $PI \ge 4$ and plots on or above "A" line.
- ^o PI < 4 or plots below "A" line.
- ^P PI plots on or above "A" line.
- ^Q PI plots below "A" line.



APPENDIX D SUSTAINABILITY CONSIDERATIONS

SUSTAINABILITY CONSIDERATIONS

LEED Sustainable Sites (SS)

SS Prerequisite 1 – Construction Activity Pollution Prevention

The intent is to reduce pollution from construction activities by controlling soil erosion, waterway sedimentation and airborne dust generation. Terracon can assist in developing site specific Storm Water Management Plans (SWMP's) in addition to providing observation services for the duration of the project for conformance to the SWMP's.

SS Credit 5.1 - Site Development – Protect or Restore Habitat

The intent is to conserve existing natural areas and restoring damaged areas to provide habitat and promote biodiversity. Terracon can provide restoration recommendations such as design of mechanically stabilized earth vegetative faced retained slopes, stream mitigation, etc.

SS Credit 6.1 and Credit 6.1 – Storm Water Design – Quantity Control and Quality Control

Sustainable storm water design limits disruption of natural hydrology by reducing impervious cover, increasing on-site infiltration, and managing storm water runoff. Terracon can provide design recommendations for porous pavement systems and infiltration basins to assist in maintaining pre-development peak discharge rates of design storms without compromising the structural capacity of the pavement or surrounding improvements. A pervious pavement system is a pavement that is sufficiently porous to allow the infiltration of water into a sub-drainage system or open-graded aggregate base reservoir below paved areas. The collected water is allowed to infiltrate through a filter fabric into the underlying subgrade soils or the water is collected and discharged to a suitable outlet.

LEED Energy and Atmosphere (EA)

EA Credit 2 – On-site Renewable Energy

The intent is to provide on-site renewable energy. Self supply renewable energy potentials Include horizontal and vertical loop fields. Terracon can provide thermal resistivity testing for horizontal loop fields or trial testing for vertical geothermal wells.

LEED Materials and Resources (MR)

MR Credit 2 – Construction Waste Management

The intent is to divert construction and demolition debris from disposal in landfills and incineration facilities.

<u>Reuse of On-Site Building Materials or Construction Debris:</u> Reusing inorganic building materials derived from foundation demolition or construction debris as processed fill material is acceptable provided the materials are crushed to a well-graded homogenous mixture and free of wood and other deleterious debris. Crushed concrete foundations, flatwork and brick may be incorporated into structural compacted fill in approved areas.

Maximum size of crushed material should be no greater than 3 inches. Use of fill materials will depend upon the source of the recycled material and the intended use. Materials such as wood and metal should be properly disposed off-site. *Caution should be used when specifying painted recycled materials. In some states, the paint would need to be analyzed to evaluate if it is lead-based. The text above may need to be edited to say "uncoated" building materials*

<u>Use of On-site Crushed Asphaltic Cement Concrete (ACC) Pavement for Engineered Fill:</u> ACC pavement, and the underlying base rock can be used as engineered fill as long as it is properly processed. It is important that the recycled ACC pavement be blended with another material, such as soil, sand, and/or gravel, to fill voids. This material should be well graded and have a maximum size, in any dimension, of 6-inches. This may necessitate the use of on-site screening of the materials and processing the oversized portion through a crusher such that the maximum size of the well graded blend would be 6-inches.

Recycled ACC pavement should be limited to a maximum of 50% of the fill material being placed in any lift. This material should be used deep within the fill or in non-structural areas such that it does not underlie future excavations being made for footings, utilities, etc.

MR Credit 4 – Recycled Content

<u>Flowable Fill:</u> Consider using flowable fill for trench backfill. The flowable fill should be comprised of waste materials such as waste limestone screenings as the bulk-filler and fly-ash for the cementitious component.

<u>ACC Pavement:</u> ACC Pavement produced in the Central Florida area typically includes 20 percent recycled asphalt pavement (RAP) and 4 percent recycled asphalt shingles resulting in a product that contains 24% recycled material.

Limestone Screenings (Waste Lime): Limestone screenings are a waste product produced by many Central Florida Quarries. This material is usually wasted in the quarries if it does not possess enough calcium content to be suitable for ag-lime applications and also because there is more product produced than demand can satisfy. As a result, this material is abandoned on-site as a waste product. This material typically is well graded crushed aggregate material with an approximate top size of ¼-inch. This material can be used as engineered fill material in structural and non-structural areas of the project. The limestone screenings can be used for the low volume change zones as a suitable replacement for shrink/swell prone soils.

<u>Supplementary Cementitious Materials (SCM's):</u> Consider using SCM's that are recycled from other operations, such as fly ash, in concrete mixes.

<u>Soil Subgrade Stabilization:</u> Consider using Fly-Ash or Code-L (a waste by-product produced when making cement) to stabilize or otherwise improve the soil subgrade.

MR Credit 5: Regional Materials

Using regional materials is intended to increase demand for building materials and products that are extracted and manufactured within the region. Regional materials also reduce environmental impacts caused by transportation.

<u>Asphaltic Cement Pavement (ACC)</u>: ACC pavement is typically produced locally. Asphalt and aggregates are typically derived locally. Oils may or may not be derived locally.

<u>Portland Cement Concrete (PCC):</u> PCC is typically derived locally including sand, gravel, water, and cement. Additives may or may not be locally derived.

<u>Aggregates for Base and Backfill:</u> Coarse and fine aggregates are typically derived locally from quarrying operations or from dredging operations.

National Pollutant Discharge Elimination System Groundwater Testing and Database Search

Greenview Pines Pump Station No. 3887 3955 Greenview Pines Court, Orlando Orange County, Florida

October 4, 2012 Nodarse/Terracon Project No. AK125005

Prepared for: Orange County Public Utilities-Engineering Division Orlando, Florida

Prepared by:

Nodarse & Associates, Inc. A Terracon Company Winter Park, Florida 32789

Offices Nationwide Employee-Owned nodarse.com terracon.com





October 4, 2012

Orange County Utilities Department Engineering Division 9150 Curry Ford Road Orlando, Florida 32825

- Attn: Mr. Heriberto Collado-Lopez, P.E. Phone: 407-254-9900 Fax: 407-254-9999
- Re: Groundwater Sampling/Testing National Pollutant Discharge Elimination System (NPDES) Parameters Greenview Pines Pump Station No. 3887 3955 Greenview Pines Court, Orlando, Orange County, Florida Nodarse/Terracon Project No. AK125005

Dear Mr. Collado:

In accordance with your request and authorization, Nodarse & Associates, Inc., a Terracon Company (Nodarse/Terracon), has completed National Pollutant Discharge Elimination System (NPDES) groundwater quality sampling and testing services at the above referenced location in accordance with our proposal number PH1120208 dated May 2, 2012, and Orange County Purchase Order #C11903A011, dated July 11, 2012.

A review of the Florida Department of Environmental Protection's (FDEP's) Contamination Locator Database website did not reveal the presence of any identified contaminated site within 1,000 feet of the project site.

On September 19, 2012, a temporary monitor well (TMW-4) was installed by direct-push Geoprobe drilling method to a depth of 15 feet below land surface (BLS). The depth to the shallow water table was measured at 4.1 feet BLS. On September 20, 2012, after well purging and stabilization of groundwater field parameters, Nodarse/Terracon collected one representative groundwater sample (PS #F3887) for laboratory testing. The groundwater sample was delivered to Southern Research Laboratories, Inc. (SRL) of Orlando, Florida (Florida Department of Health #E83484) for analysis of NPDES parameters.

As shown in Table 1, the reported concentration of one parameter, total organic carbon (TOC), detected at 16 milligrams per liter (mg/l), exceeded the Chapter 62-621.300 (2), Florida Administrative Code, listed screening value (LSV) of 10 mg/l. The elevated TOC value is likely attributable to naturally-occurring, high molecular weight organic compounds in the groundwater at this location. This is confirmed by the reported non-detection of total recoverable petroleum

Winter Park, Florida 32789



Nodarse & Associates, a Terracon Company 1675 Lee Road



hydrocarbons (TRPH) above the laboratory method detection limit in the groundwater sample. Field pH was measured at 5.01 standard units (SU), which is below the LSV range of 6.5 - 8.0 SU. The measured field pH is representative of background pH levels below 6.0 (acidic) in east Orange County. The remaining parameters analyzed did not report exceedances above their respective LSVs.

A copy of the laboratory analytical report, the groundwater sampling log, instrument calibration sheet, the monitoring well details and a site photograph are included in Appendix A.

Nodarse/Terracon appreciates the opportunity to have assisted with these services if you should have any questions or comments, please feel free to contact us.

Sincerely, Nodarse & Associates, Inc., a Terracon Company

Hardo

Project Environmental Scientist

John Malkowski, P.E. Con Florida License No. 59404 Senior Engineer

N:\Projects\2012\AK125005\PROJECT DOCUMENTS (Reports-Letters-Drafts to Clients)\NPDES Greenview Pines\AK125005 Final NPDES Report.doc

TABLE

TABLE 1

GROUNDWATER ANALYTICAL SUMMARY FINAL RESULTS OF NPDES CONCENTRATIONS GREENVIEW PINES PUMP STATION #3887 ORLANDO, ORANGE COUNTY, FLORIDA NODARSE/TERRACON PROJECT NO. AK125005 SAMPLING DATE: SEPTEMBER 20, 2012

	Sample ID		
PARAMETER	PS #F3887	Limits*	Units
DATE SAMPLED	09/20/12	Limits	Units
Benzene	0.5 U	1.0	μg/L
Naphthalene	0.10 i	100	μg/L
Cadmium, Total	0.306 U	9.3	μg/L
Copper, Total	1.40 U	2.9	μg/L
Lead, Total	1.60 U	30.0	μg/L
Mercury, Total	0.00288	0.012	μg/L
Zinc, Total	47.2 v	86.0	μg/L
Chromium, Hexavalent	4.2 U	11.0	μg/L
Total Organic Carbon (TOC)	16	10.0	mg/L
TRPH	200 U	5000.0	μg/L
pH - Field	5.01	6.0 - 8.5	μg/L
Turbidity	1.38	NA	NTU

NOTES:

Bold values represent a concentration exceeding the respective NPDES criteria

mg/L - milligrams per liter

µg/L - micrograms per liter

i - indicates value < method detection limit but > than practical quantitation limit

I - The reported concentration is between the MDL and PQL

U - not detected above method detection limit

v - Analyte was detected in both the sample and associated Lab Method Blank; laboratory contamination

* Based on the Florida Department of Environmental Protection' s Effluent Discharge

Generic Dewatering Permit Table 4 Screening Values (Doc # 62-621.300(1), eff. 2-14-2000

NS - No applicable limitation or standard referenced

NA - Not applicable

APPENDIX A

LABORATORY ANALYTICAL REPORT, GROUNDWATER SAMPLING LOGS, INSTRUMENT CALIBRATION SHEET, MONITORING WELL DETAILS AND PHOTOGRAPH



2251 Lynx Lane, Suite 1 Orłando, Florida 32804 (407) 522-7100 Fax (407) 522-7043 Toll Free 1 (888) 420-Test

Thank you **Mr. Ed Sainten** for the opportunity to be of service to you and your company; we Sincerely Appreciate Your Business. SRL certifies these **Laboratory Results** were produced in accordance with NELAC Standards. Hold times and preservation requirements were met for all analytes unless specifically noted in the report. Results relate only to the samples as received.

Client Name: Te	rracon		Date(s) Collected: 09/20/12	
Contact Name: E	d Sainten		Date Received: 09/20/12	
Project Name: G	reenview Pines PS #3387		Time Received: 13:08	
Project Number:	AK-12-5005		Date Reported : 09/28/12	
Phone Number: ((407) 740-6110		Date Emailed : 09/28/12	
Fax Number: (40	07) 740-6112	SRL Work Order # 12-09025		
SRL WO #	Clients #	Matrix	Analysis Requested	
12-09025-001	PS #F3887	Liquid	EPA8260(Benz)/TOC/Cd/Cu/Pb/Zn/ 8270-SIM(PAH)Naph/FLPRO/ LL Hg/Hexavalent Chromium	
12-09025-002	Trip Blank	Lìquid	EPA 8260 (Benz)	



Sherri Paync Vice President & Quality Assurance Officer Southern Research Laboratories, Inc.

This report, which includes the attached Chain-of-Custody, shall not be reproduced except in full, without written approval of the laboratory.

Southern Research Laborato	ries, Inc.	NELAP Certified			
an MBE Environmental Labor	ratory	FDOH Cert # : E83484			
2251 Lynx Lane, Suite 1		SRL Lab Ref # : 12-09025			
Orlando, Florida 32804	(407) 522-7100	Received Date : 09/20/12			
Ed Sainten		Project Number/Project Name			
Terracon		AK-12-5005			
1675 Lee Rd.		Greenview Pines PS #3387			
Winter Park, FL 32789	(407) 740-6110	Orlando, FL			

EPA Method 5030/8260B VOA {602} Compounds in Water by GC-MS

Client ID #	:	PS #F3887	Trip Blank	Method Blank			
SRL (Lab) ID#	:	12-09025-001	12-09025-002	MB092512			
Date Collected	:	09/20/12	09/18/12	NA			
Lab FDOIL Certification #	:	E83484	E83484	E83484			
Date Prepared	:	09/25/12	09/25/12	09/25/12			
Date Analyzed	:	09/25/12	09/25/12	09/25/12	MDL	PQL	CAS Number
Benzene		0.5 U	0.5 U	0.5 U	0.5	1.0	71-43-2
Units	:	ug/L	ug/L	ug/L	ug/L	ug/L	
Dilution Factor (MEDF)	:	1	1	1	1	1	
Surrogate (% Rec)	:				(Surrogat	e Contro	ol Limits)
4-Bromofluorobenzene		92.2%	97.7%	95.0%		70-130	
			LCS	MS/MSD			

		LUS	W13/W13D		
	% Recovery	Acceptable	Acceptable	%RPD	Acceptable
	LCS/MS/MSD	Limits	Limits	MS/MSD	Limits
Benzene	109/81/81	70-130	70-130	0.5	0-30

EPA Method 3510/8270C-SIM Polynuclear Aromatic Hydrocarbon Compounds +Naph in Water by GC-MS

Client ID #	: PS #F3887	Method Blank				
SRL (Lab) ID#	: 12-09025-001	MB092512				
Date Collected	: 09/20/12	NA				
Lab FDOH Certification #	: E83484	E83484				
Date Extracted	: 09/25/12	09/25/12				
Date Analyzed	: 09/26/12	09/26/12		MDI	<u> </u>	CAS Number
Naphthalene	0.10 I	0.10 U		0.10	0.50	91-20-3
Units	: ug/L	ug/L		ug/L	ug/L	
Dilution Factor (MEDF)	: 1	1		1	1	
Surrogate (% Rec)				(Surrog	ate Contro	ol Limits)
Nitrobenzene-D5	79.9%	87.3%			60-140	
2-Fluorobiphenyl	85.2%	74.6%			60-140	
p-Terphenyl-D14	98.9%	105.2%			60-140	
	% Recovery LCS/MS/MSD		%RPD MS/MSD	Acceptable Limits		
Naphthalene	83/76/82	60-140	7.6	30		

Southern Research Laborato an MBE Environmental Labor						P Cert	ified : E83484	
2251 Lynx Lane, Suite 1	uloy							
Orlando, Florida 32804	(407) 522-710	00			SRL Lab Ref # : 12-09025 Received Date : 09/20/12			
Ed Sainten					Proiec	t Numbe	er/Project Name	
Terracon					AK-12		on a reget raine	
1675 Lee Rd.							nes PS #3387	
Winter Park, FL 32789	(407) 740-611	0				do, FL	lites 1 6 #5567	
winter Park, FL 52769	(407) 740-01	0			Oriali	uo, rL		
	<u>FL-PRO (P</u>	etroleum Range	Organics)~{V	Water}				
Client ID #	: PS #F3887	Method Blank						
SRL (Lab) ID#	: 12-09025-001	MB092612						
Date Collected	: 09/20/12	NA						
Lab FDOH Certification #	: E83484	E83484						
Date Prepared	: 09/26/12	09/26/12						
Date Analyzed	: 09/27/12	09/27/12			MDL	_PQL	CAS Number	
TOTAL PRO (C8-C40)	0.2 U	0.2 U			0.2	0.5	NΛ	
Units	: mg/L	mg/L			mg/L	mg/L		
Dilution Factor (MEDF)	: 1	[1	1		
Surrogate (% Rec)	:	115 50/			(Surroga		ol Limits)	
Orthoterphenyl (OTP)	102.5%	115.7%				82-142		
	% Recovery	Acceptable	%RPD	Acceptabl	c			
	LCS/LCSD	Limits	LCS/LCSD	Limits				
TOTAL PRO (C8-C40)	84/85	55-118	1.7	0-20				
	Hexavalent Ch	romium by SM	18 3500-Cr D	in Water				
Client ID #	: PS #F3887	Method Blank						
SRL (Lab) ID#	: 12-09025-001	MB092012						
Date Collected	: 09/20/12	NA						
Lab FDOH Certification #	: E83182	E83182						
Date Prepared	: 09/20/12	09/20/12						
Date Analyzed	: 09/20/12	09/20/12						
Time Analyzed	: 22:21	22:09						
Units	: mg/L	mg/L			MDL		CAS Number	
Hexavalent Chromium	0.0042 U	0.0042 U			0.0042	0.030	1854-02-99	
		LCS	MS/MSD					
	% Recovery	Acceptable	Acceptable	%RPD	А	cceptab	le	
	LCS/MS/MSD	Limits	Limits	MS/MSD		Limits		
Haussia fant Clauser fun	10(/02/02	05 115	05 115	^		0.10		

Hexavalent	Clưomium
------------	----------

LCS/MS/MSD Limits 106/92/93 85-115

85-115

MS/MSD 2

0-13

Southern Research Laborato an MBE Environmental Labor 2251 Lynx Lane, Suite 1 Orlando, Florida 32804	,	0			FDOH SRL L	ab Ref i	ified : E83484 # : 12-09025 : : 09/20/12
Ed Sainten Terracon 1675 Lee Rd. Winter Park, FL 32789	(407) 740-611	0			AK-12 Green	-5005	er/Project Name nes PS #3387
	<u>Total Organi</u>	e Carbon by SM	<u>118 5310B in</u>	Water			
Client ID # SRL (Lab) ID# Date Collected Lab FDOH Certification # Date Prepared Date Analyzed Dilution Factor (MEDF) <u>Units</u> Total Organic Carbon (TOC)	: PS #F3887 : 12-09025-001 : 09/20/12 : E83182 : 09/26/12 : 09/26/12 : 1 : mg/L 16	Method Blank MB092612 NA E83182 09/26/12 09/26/12 1 mg/L 0.22			<u>MDL</u> 0.22	PQL 1.0	<u>CAS Number</u> ECL-0165
Total Organic Carbon (TOC)	10	0.22			0.22	1.0	ECT-0102
Total Organic Carbon (TOC)	% Recovery LCS/MS/MSD 100/103/104	Acceptable Limits 85-115	%RPD MS/MSD 0.7	Acceptable Limits 0-21			
	EPA Method 16	31 Low Level N	Mercury (Hg)	in Water			
Client ID # SRL (Lab) ID# Date Collected Lab FDOH Certification # Date Prepared Date Analyzed Units Low Level Mercury (Hg)	: PS #F3887 : 12-09025-001 : 09/20/12 : E87688 : 09/24/12 : 09/25/12 : ng/L 2.88	Method Blank MB092412 NA E87688 09/24/12 09/25/12 ng/L 0.183 U			MDL 0.183	PQL 0.5	<u>CAS Number</u> 7439-97-6
Low Level Mercury (Hg)	% Recovery LCS/MS/MSD 107/100/91	LCS Acceptable Limits 77-123	MS/MSD Acceptable Limits 71-125	%RPD MS/MSD 8.7		cceptab Limits 0-24	

Southern Research Laborato	pries, Inc.	NELAP Certified			
an MBE Environmental Labo	ratory	FDOH Cert # : E83484			
2251 Lynx Lane, Suite 1		SRL Lab Ref # : 12-09025			
Orlando, Florida 32804	(407) 522-7100	Received Date : 09/20/12			
Ed Sainten		Project Number/Project Name			
		AK-12-5005			
Terracon		AK-12-5005			
Terracon 1675 Lee Rd.		AK-12-5005 Greenview Pines PS #3387			
	(407) 740-6110				

Metals (total recoverable) by EPA 200 Series Methods

Client ID #	: PS #F3887	Method Blank	
SRL (Lab) ID#	: 12-09025-001	MB092412	
Date Collected	: 09/20/12	NA	
Lab FDOH Certification #	: E82277	E82277	
Date Prepared	: 09/24/12	09/24/12	
Date Analyzed	: 09/25/12	09/25/12	
Units	: ug/L	ug/L	MDL PQL CAS Number
Cadmium	0.306 U	0.306 U	0.306 1.00 7440-43-9
Copper	1.40 U	1.40 U	1.40 10.0 7440-50-8
Lead	1.60 U	1.60 U	1.60 10.0 7439-92-1
Zinc	47.2 V	* 7.86 I	3.00 10.0 7440-66-6

		LCS	MS/MSD		
Prep. Method EPA 3005A	% Recovery	Acceptable	Acceptable	%RPD	Acceptable
EPA 200.7	LCS/MS/MSD	Limits	Limits	MS/MSD	Limits
Cadmium	104/102/102	85-115	70-130	0.1	0-25
Copper	101/101/101	85-115	70-130	0.2	0-25
Lead	102/100/100	85-115	70-130	0.7	0-25
Zinc	99/98/97	85-115	70-130	0.7	0-25

* This compound is a common laboratory contaminant

Southern Research Laborato	ries, Inc.	NELAP Certified		
an MBE Environmental Labor	ratory	FDOH Cert # : E83484		
2251 Lynx Lane, Suite 1		SRL Lab Ref # : 12-09025		
Orlando, Florida 32804	(407) 522-7100	Received Date : 09/20/12		
Ed Sainten		Project Number/Project Nam		
Terracon		AK-12-5005		
1675 Lee Rd.		Greenview Pines PS #3387		
Winter Park, FL 32789	(407) 740-6110	Orlando, FL		

DATA QUALIFIER CODES

Reporting Exceptions and Qualified Data

When quality control results are outside established control limits reanalysis, including re-extraction (if applicable), is preferred. If re-analysis is not viable or desirable, then results may be qualified. Sample results associated with quality control data that exceed acceptance criteria will be qualified with an appropriate comment.

- $\mathbf{D} = \mathbf{D}$ ata reported from a dilution and or multiple dilutions.
- I = Estimated Value, The reported value is between the Laboratory Method Detection Limit (MDL) and the Laboratory Practical Quantitation Limit (PQL)
- $\mathbf{J} = Estimated Value$
- L = Off-Scale high; exceeds the linear range or highest calibration standard.
- O = Sampled, but analysis lost or not performed
- $\mathbf{Q} =$ Sample held beyond normal holding time
- U = indicates the compound was analyzed for, but not detected. The numerical value preceding the "U" is the limit of detection for that compound based upon the dilution. MEDF = Matrix Effected Dilution Factor.
- V = Analyte was detected in both the sample and associated Laboratory Method Blank; Laboratory Contamination
- $\mathbf{Y} =$ The analysis was from an unpreserved or improperly preserved sample. The data may not be accurate

Unless otherwise noted, ug/Kg and mg/Kg denote dry weight.

(SOILS) Actual Reporting Limit will depend on moisture content of sample and the amount of sample received.

LCS Obs. Value is the observed quantity, as calculated from the calibration curve, of the analyte in the Laboratory Control Sample (LCS). The LCS is a standard from a source different than the source of the standards used for calibration. The LCS is also known as the QC sample. It is used to check the accuracy of the calibration curve.

There are the solution for the point of the	7 C Matrix: (see C Matrix: (see 2 C Matrix: (s	E TERPHONEN	Hex Chremium H	Ev PBE
Flair 32795 Flair 32795 Flair 510 Flair 5279 Flair 5279 Flair 5279 Flair 5279 Flair 1132 Flair	10 Touristication 10 10 10 10 10 10 10 10 10 10 10 10 10	I How How How I was	B B H MUIMONAD XOH	AIL Projust N
+1 (ample on Sampled Composite 13 / Terration 13 / 13 / 13 / 13 / 13 / 13 / 13 / 13	18 18 10 10 10 10 10 10 10 10 10 10	T Kiphthalen	A H MUIMONAD XOH	The second second
1. Affiliation 2. Terrescon 2. 1. Errescon Data Sampled Data Taan Composite Compos	in redination of the second of	I Hold Phyloder	н	Project Number: AIL 12 - 5005 REQUESTED DUE DATE: Standard Sampling QAP No
Miller Durins / Terricon Miller Durins / Terricon Mull. Dury Mull. Dury Data Then PS-HE-3887 9/20/12 1132 Crab PS-HE-3887 9/20/12 1132 Crab	to reaction of Contractions	I Hold I w	H history	A14 12 - 5005 REQUESTED DUE DATE: Sampling QAP No
M.L. Dur M.L. Dur Sample Identification Sampled Data Tau Th. J. M.L. Dur Data Tau Th.J. M.L. Dur Data Tau Th.J. M.L. Dur Data Tau Th.J. M.L. Dur Data Tau	to reducing the of the	НАЯТЯ	LE MERENY	REQUESTED DUE DATE: Stradard Sampling QAP No
W. D. D. Sample laboration Sample laboration DSHE2387 912.12 1132 Composite The p Blinnes P. 12 2 1.12	A O Total fumber of	8 TRPH	LL MERCUN	Standard Sampling QAP No
Sample lacatification Sample lacatification DSzt 7 2887 9/20/12 1132 Crabs II 7 D. 17 12/12 21:12 21:12	Couldinate of	R TRPH	LL WELEN	Sampling QAP No.
Parts The The Construction of the PSHE 2887 9120 1132 Crab Construction of the PSHE 2112 1132 Crab Construction of the PSHE 2112 2112 1132 Crab Construction of the PSHE 2112 2112 2112 2112 2112 2112 2112 21	1 Tours	AT &	77	Approval Dute:
PS±F=3887 9/20/12 1132 Grab They Blank Surie 21:12 -	10	3	1	Coentents:
72.17 Blinde Gist 28.12 -	P -		(S) (S)	1205025-001
				Em-
				,
Chinement Markov.	Traditional houses in the statement			Active Ac
		5	Milber.	0/20/15 0
Returned + +	15.21 B	2/2-/12 1/302	1212	9-20.12 8308
Casher Narga / T	Cooler No. (a) / Tamperature(s) ('U'):	Sampling Kit No.	s 523	Equipment ID Nu.:

Form FD 9000-24 **GROUNDWATER SAMPLING LOG**

SITE /		0		+	si	TE		A		Kise	- 2.9'
				F-388	1 LC		Orland	به ۲۰۰٬			
WELL NO:	: ps ≠ _f	23887		SAMPLI	EID: PS	# F3	887		DATE: 9/	20/12	
					PUR	GING DA					
	R (Inches):		G TER (inches):	1/8 11 WE		INTERVAL				ge pump tyf Bailer: 🛛 🗡	РЕ 2, рЭ
WELL VO	LUME PURGE	: 1 WELL VO	LUME = (TOT	AL WELL DE	PTH – STA	TIC DEPTH	TO WATER) X	WELL CAPACI	TY		
(only fill or	ut if applicable)		= (7.4	feet -	7.03	feet) X	JBING LENGTH)	gallons/foot	=0,4	3 gallo
		URGE: 1 EQ	JIPMENT VOL	= PUMP VO	LUME + (TUE	SING CAPACI	ד א אדו	JBING LENGTH)	+ FLOW CEL	L VOLUME	
(only fill of	it if applicable)			= g	allons + (ons/foot X	feet)	+	gallons =	gallo
	UMP OR TUBIN WELL (feet):	^{IG} 13,0	FINAL PUN DEPTH IN	IP OR TUBIN WELL (feet): /	G 15.9		IG ED AT: 11/0		1132	TOTAL VOLU PURGED (ga	IME Ilons): 1.3
TIME	VOLUME PURGED (gallons)	CUMUL. VOLUME PURGED (gallons)	PURGE RATE (gpm)	DEPTH TO WATER (feet)	pH (standard units)	TEMP. (°C)	COND, (circle units) nhos/cm or S/cm	DISSOLVED OXYGEN (circle units) OgA or Wosaturation	TURBIDITY (NTUs)	COLOR (describe	
1117	0,43	0.43	,04	19.87	5,01	2685	93	58.6%/0/4.66	11.2	Clear	jon
1120	0.18	0.61		14.03	4,81	26.92	76	51.2% 4,02		CL	L,
1/23	0,18	0,79		14.37	4.71	26.82	80	49,40/0/3,94		CL	11
126	0.18	0.97		14.84	4.65	26,82	74	46.7% 3:33		CL	1.
121	0,18	1.15		14.89	4.60	26,81	75	45,10/0/3,57		CL	81
132	0.18	1.3 3	1	14,94	4,57	26.82	76	44.4% 3.55	1.38	ĊĊ	L #
	PACITY (Gallor NSIDE DIA. CA								5" = 1.02;		2" = 5.88 8" = 0.016
PURGING	EQUIPMENT	CODES: B	= Bailer;	BP = Bladder			Submersible Pu	mp; PP = Pe	ristaltic Pump	; O = Oth	er (Specify)
			1	SAMPLER(S		LING DA				1	
	BY (PRINT) /		I		1 Bit			SAMPLING INITIATED AT	1132	SAMPLING ENDED AT	hou
		1 2 2 2 3 3 3									
Mike PLIME OR	TUBING				P	15/2		-FILTERED: Y		FILTER SIZ	E: m
PUMP OR DEPTH IN	TUBING WELL (feet):	15,0	ل	TUBING MATERIAL C			Filtratio	-FILTERED: Y	e:		E: m
PUMP OR DEPTH IN FIELD DE	TUBING WELL (feet): CONTAMINATI	15,0 ON: PUM	lP Y &		TUBING	Y DOW	Filtration (Filtration)	-FILTERED: Y on Equipment Typ DUPLICATE:	Y	8	
PUMP OR DEPTH IN FIELD DE	TUBING WELL (feet):	15,0 ON: PUM	lP Y &	TUBING MATERIAL C	TUBING SAMPLE PF		Filtration Phaced) N FINAL	-FILTERED: Y	Pe: Y D SA ID/OR EQ		SAMPLE PU
PUMP OR DEPTH IN FIELD DEC SAM	TUBING WELL (feet): CONTAMINATI PLE CONTAIN	0N: PUN ER SPECIFIC/ MATERIAL		TUBING MATERIAL C	TUBING SAMPLE PF	Y MARESERVATIO	Filtration Phaced) N FINAL	-FILTERED: Y an Equipment Typ DUPLICATE: INTENDE ANALYSIS AN	D SA ID/OR EQ	MPLING UIPMENT CODE	SAMPLE PU FLOW RAT (mL per minu
Miles PUMP OR DEPTH IN FIELD DEC SAM SAMPLE ID CODE	TUBING WELL (feet): CONTAMINATI PLE CONTAIN CONTAINERS 2. 2. 2.	NN: PUN ER SPECIFIC/ MATERIAL CODE C & AG	ATION VOLUME	TUBING MATERIAL C PRESERVAT USED	TUBING SAMPLE PF	Y MARESERVATIO	Piltration eplaced) N mL) FINAL pH	FILTERED: Y on Equipment Typ DUPLICATE: INTENDE ANALYSIS AN METHOD	D SA ID/OR EQ	€ MPLING UIPMENT CODE E pp	SAMPLE PUł FLOW RAT (mL per minu くしひゅ ん
Miles PUMP OR DEPTH IN FIELD DEC SAM SAMPLE ID CODE	UBING WELL (feet): CONTAMINATI PLE CONTAIN: # CONTAINERS 2-	NS PUN ER SPECIFIC/ MATERIAL CODE CC AG CC	IP Y & ATION VOLUME COMC	TUBING MATERIAL C PRESERVAT USED 14°C C	TUBING SAMPLE PF	Y MARESERVATIO	Piltration eplaced) N mL) FINAL pH	FILTERED: Y on Equipment Typ DUPLICATE: INTENDE ANALYSIS AN METHOD U-0,4 TOC L L Mur	Y D SA ID/OR EQ D K/	MPLING UIPMENT CODE	SAMPLE PUR FLOW RAT (mL per minu Cloy M
Miles PUMP OR DEPTH IN FIELD DEC SAM SAMPLE ID CODE	TUBING WELL (feet): CONTAMINATI PLE CONTAIN CONTAINERS 2. 2. 2.	NN: PUN ER SPECIFIC/ MATERIAL CODE CC AG AG	IP Y X ATION VOLUME GOMC GOMC GOML GOML GUTT,	TUBING MATERIAL C PRESERVAT USED 14C C Mone HCC Mone	TUBING SAMPLE PF	Y MAR RESERVATIO TOTAL VOL D IN FIELD (Filtration eplaced) iN mL) FINAL pH	FILTERED: Y on Equipment Typ DUPLICATE: INTENDE ANALYSIS AN METHOD UPO A TOC L L Mer 8270 SIM	Y ID SA ID/OR EQ D ID/OR ID/OR ID/OR <		E: m SAMPLE PUN FLOW RATI (mL per minu (mL per minu (mL por minu (mL por minu (mL por minu (mL por minu (mL por minu (mL por minu)
Miles PUMP OR DEPTH IN FIELD DEC SAM SAMPLE ID CODE	TUBING WELL (feet): CONTAMINATI PLE CONTAIN CONTAINERS 2. 2. 2. 2.	NS: PUN ER SPECIFIC/ MATERIAL CODE CC AG AG AC	ATION VOLUME GOMC GOMC GOMC GML LLT, ILT,	TUBING MATERIAL C PRESERVAT USED 14CC Mone HCC	TUBING SAMPLE PF	Y MARESERVATIO	Filtration eplaced)	FILTERED: Y on Equipment Typ DUPLICATE: INTENDE ANALYSIS AN METHOD UCOA TOC LLMER 8270 SIM	PE: Y ID/OR C. PAUI		SAMPLE PUR FLOW RAT (mL per minu (100 M (100 M) (100 M)
PUMP OR DEPTH IN FIELD DEC SAM SAMPLE ID CODE	TUBING WELL (feet): CONTAMINATI PLE CONTAINS CONTAINERS 2. 2. 2. 2. 2. (((1	IS, C ON: PUN ER SPECIFIC/ MATERIAL CODE CG AG AG AG AC FE	ATION VOLUME GOMC GOMC GOML GOML LLT, ZJOMC	TUBING MATERIAL C PRESERVAT USED 14C C Mone HCC Mone MCC		Y MAR RESERVATIO TOTAL VOL D IN FIELD (Filtration eplaced)	FILTERED: Y on Equipment Typ DUPLICATE: INTENDE ANALYSIS AN METHOD UCOA TOC LLMER 8270 SIM	PE: Y ID/OR C. PAUI		SAMPLE PUI FLOW RAT (mL per minu Lion M Lion M Lion M
Miles PUMP OR DEPTH IN FIELD DEC SAM SAMPLE ID CODE	TUBING WELL (feet): CONTAMINATI PLE CONTAINS CONTAINERS 2. 2. 2. 2. 2. (((1	IS, C ON: PUN ER SPECIFIC/ MATERIAL CODE CG AG AG AG AC FE	ATION VOLUME GOMC GOMC GOMC GML LLT, ILT,	TUBING MATERIAL C PRESERVAT USED 14CC Mone HCC Mone Mone MCC		Y MAR RESERVATIO TOTAL VOL D IN FIELD (Filtration eplaced)	FILTERED: Y on Equipment Typ DUPLICATE: INTENDE ANALYSIS AN METHOD UPO A TOC L L Mer 8270 SIM	PE: Y ID/OR C. PAUI		SAMPLE PUR FLOW RAT (mL per minu (100 M (100 M) (100 M)
PUMP OR DEPTH IN FIELD DEC SAM SAMPLE ID CODE	TUBING WELL (feet): CONTAMINATI PLE CONTAINERS Z. Z. Z. (((1 S: (NS. PUN ER SPECIFIC/ MATERIAL CODE C.C. A.C. A.C. P.E. P.E.	ATION VOLUME GOMC GOMC GOML GOML LLT, ZJOMC	TUBING MATERIAL C PRESERVAT USED 14C C Mone HCC Mone HCC Mone HCC	TUBING SAMPLE PF IVE ADDE	Y MAR RESERVATIO TOTAL VOL D IN FIELD (Filtration eplaced)	FILTERED: Y on Equipment Typ DUPLICATE: INTENDE ANALYSIS AN METHOD UCOA TOC LLMER 8270 SIM	$\begin{array}{c c} & & & \\ & & & & \\ & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & &$	€ MPLING UIPMENT CODE E PP A A A A A A A A A A A A A A A A A	SAMPLE PUR FLOW RAT (mL per minu (100 M (100 M) (100 M)

The above do Not constitute an of the information required by Chapter 92-100, F.A.C.
 STABILIZATION CRITERIA FOR RANGE OF VARIATION OF LAST THREE CONSECUTIVE READINGS (SEE FS 2212, SECTION 3)
 pH: ± 0.2 units Temperature: ± 0.2 °C Specific Conductance: ± 5% Dissolved Oxygen: all readings ≤ 20% saturation (see Table FS 2200-2); optionally, ± 0.2 mg/L or ± 10% (whichever is greater) Turbidity: all readings ≤ 20 NTU; optionally ± 5 NTU or ± 10% (whichever is greater)

DEP-SOP-001/01 FT 1000 General Field Testing and Measurement

	Form	n FD 9000	-8: FIEL	D INSTRUME	NT CALI	BRATION R	ECORDS	
INSTRUM	ENT (M/	AKE/MOD	EL#)	YSI 556MF	PS	INSTRUM	ENT # 06H	2510AF
PARAME	TER: [cl	heck only	one]					
🗌 TEM	PERATUR	RE 🔀	CONDUC	rivity 🗌 s	SALINITY	🕅 pH	ORP	
🗌 TUR	BIDITY		RESIDUAI	_CI 🔀 🛛	00	🗌 OTH	ER	
values, and	the date th	ne standards	were prep	ndards used for c ared or purchased		he origin of the	standards, the	standard
		Do 1						
Standa	ard B	PH	4,7,	0				
		Conducti						
DATE (yy/mm/dď)	TIME (hr:min)	STD (A, B, C)	STD VALUE	INSTRUMENT RESPONSE	% DEV	CALIBRATED (YES, NO)	TYPE (INIT, CONT)	SAMPLER INITIALS
9/20/12	0925	A	100%	92,0 /100,3	8%/21	Yes	Init	mb
ľ	0934	B	4,0	4.03	Z 1			
	0943	B	7.0	6.97	41	{		
	0949	B	10.0	10.10	10/0			
	0951	C	1413	1400	<1	1	1	1
9/20/12	1	A	100%	1.00.4%	<1	Yes	cont	mЬ
ĺ	1200	ß	4	4.01	41		1	1
	1203	ß	7	7,0	<(
	1208	ß	10	10.03	</td <td></td> <td></td> <td></td>			
	1211	e	1413	1413	21			
- 4	1					4	- 1	v
	-				_			
				-	_			
	_							

- Alexandre

DEP-SOP-001/01 FT 1000 General Field Testing and Measurement

	Form	n FD 9000-	8: FIEL	D INSTRUME	NT CALI	BRATION R	ECORDS	
INSTRUM	ENT (M/	AKE/MODI	EL#) <u>ŀ</u>	HACH 2100P	INST	RUMENT #	08080C017	245
PARAME	TER: [cl	heck only d	one]					
🗀 TEM	PERATUF	RE 🗍 (CONDUCT	IVITY 🗌 S	ALINITY	🗌 pH	ORP	
🗹 TUR	BIDITY		RESIDUAL		00	🗌 ОТН	ER	
				ndards used for ca ared or purchased		he origin of the	standards, the	standard
Standa	ard A	<0.1					_	
Standa	ard B	_20.0						
Standa	ard C	100						
DATE (yy/mm/dd)_	TIME (hr:min)	STD (A, B, C)	STD VALUE	INSTRUMENT RESPONSE	% DEV	CALIBRATED (YES, NO)	TYPE (INIT, CONT)	SAMPLER INITIALS
	0921	A	0,(60/10/	(25	Zait	MB.
1	1923	ß	20.0	20,2	1%)
	0925	C	100	99,3	21			
glolic	1213	Δ	0.)	0.11	10/0	405	cont	IN 17
	1214	ß	20,0	2011	LI		1	
	1215	e	1100	99.7	01			
	7010		V		_			-1
	<u> </u>							

DATE: 9/19/19 SITE: Pump Sta. # 3887 LOCATION: Orlando, FC., WELL LOCATION STRATEGY: TMW-4 DRILLING COMPANY: Groundwater Protection DRILLING METHOD / BORING DIAMETER: Geo Probe / 41' WELL DEPTH / SCREEN INTERVAL: 15' bls / 5-15' GROUNDWATER LEVEL: 7.74' BTOC TOP OF CASING ELEVATION: DEVELOPMENT PROCEDURE: Peristaltic Pump DISPOSITION OF INVESTIGATIVE DERIVED WASTES: Spread. REMARKS:

